

# Hyperbolic balance laws: Riemann invariants and the generalized Riemann problem

Matania Ben-Artzi · Jiequan Li

Received: 15 June 2006 / Revised: 5 January 2007 / Published online: 29 March 2007  
© Springer-Verlag 2007

**Abstract** The Generalized Riemann Problem (GRP) for a nonlinear hyperbolic system of  $m$  balance laws (or alternatively “quasi-conservative” laws) in one space dimension is now well-known and can be formulated as follows: Given initial-data which are analytic on two sides of a discontinuity, determine the time evolution of the solution at the discontinuity. In particular, the GRP numerical scheme (second-order high resolution) is based on an analytical evaluation of the first time derivative. It turns out that this derivative depends only on the first-order spatial derivatives, hence the initial data can be taken as piecewise linear. The analytical solution is readily obtained for a single equation ( $m = 1$ ) and, more generally, if the system is endowed with a complete (coordinate) set of Riemann invariants. In this case it can be “diagonalized” and reduced to the scalar case. However, most systems with  $m > 2$  do not admit such a set of Riemann invariants. This paper introduces a generalization of this concept: weakly coupled systems (WCS). Such systems have only “partial set” of Riemann invariants, but these sets are weakly coupled in a way which enables a “diagonalized” treatment of the GRP. An important example of a WCS is the Euler system of compressible, nonisentropic fluid flow ( $m = 3$ ). The solution of the GRP discussed here is based on a careful analysis of rarefaction waves. A “propagation of singularities” argument is applied to appropriate Riemann invariants across the rarefaction fan. It serves to “rotate” initial spatial slopes into “time derivative”. In particular, the case of a “sonic point” is incorporated

---

M. Ben-Artzi

Institute of Mathematics, The Hebrew University of Jerusalem, 91904 Jerusalem, Israel  
e-mail: mbartzi@math.huji.ac.il

J. Li (✉)

School of Mathematics, Capital Normal University, 100037 Beijing, People’s Republic of China  
e-mail: jiequan@mail.cnu.edu.cn

easily into the general treatment. A GRP scheme based on this solution is derived, and several numerical examples are presented. Special attention is given to the “acoustic approximation” of the analytical solution. It can be viewed as a proper linearization (different from the approach of Roe) of the nonlinear system. The resulting numerical scheme is the simplest (second-order, high-resolution) generalization of the Godunov scheme.

**Mathematics Subject Classification (2000)** 65M06 · 35L67 · 35L65 · 76N15

## 1 Introduction

In this paper we consider the generalized Riemann problem (GRP) for hyperbolic balance laws

$$\frac{\partial U}{\partial t} + \frac{\partial F(U)}{\partial x} = S(x, U), \quad (1.1)$$

where  $U = (u_1, \dots, u_m)^\top$  is an unknown function of  $x$  and  $t$ ,  $F = (f_1, \dots, f_m)^\top$  is the associated flux, and  $S(x, U)$  is the source term resulting from geometrical and physical effects. We develop the method of Riemann invariants in order to solve the generalized Riemann problem and derive a GRP high resolution scheme for the system. Our starting point in the present study is the associated Riemann problem, i.e., the Riemann problem for the homogeneous counterpart of (1.1), which is assumed to be solvable theoretically and numerically. We show that the Riemann invariants, which always exist for strictly hyperbolic systems of two equations (i.e.,  $m = 2$ ), play a pivotal role in the GRP solution for a large family of hyperbolic systems, including the system of shallow water equations, the compressible fluid flow (both isentropic and non-isentropic) and so on.

The GRP scheme was originally designed for compressible fluid flows [1–4]. As the extension of the Godunov scheme [9], the GRP scheme assumes piecewise smooth initial data and evolves the solution of (1.1) by analytically solving the generalized Riemann problem at each cell interface with second-order accuracy. Specifically, we denote by  $C_j = [x_{j-1/2}, x_{j+1/2}]$  ( $\Delta x = x_{j+1/2} - x_{j-1/2}$ ) the computational cell numbered  $j$ , and by  $\{t_n\}_{n=0}^\infty$  the sequence of discretized time levels,  $\Delta t = t_{n+1} - t_n$ . Assume that the data at time  $t = t_n$  is piecewise linear with a slope  $\sigma_j^n$ , i.e., on  $C_j$  we have

$$U(x, t_n) = U_j^n + \sigma_j^n(x - x_j), \quad x \in (x_{j-1/2}, x_{j+1/2}). \quad (1.2)$$

Then a Godunov-type scheme of second-order usually takes the form

$$U_j^{n+1} = U_j^n - \frac{\Delta t}{\Delta x} \left( F_{j+1/2}^{n+1/2} - F_{j-1/2}^{n+1/2} \right) + \frac{\Delta t}{2} \left( S_{j+1/2}^{n+1/2} + S_{j-1/2}^{n+1/2} \right), \quad (1.3)$$

where we use the notations

$$F_{j+1/2}^{n+1/2} = F \left( U_{j+1/2}^{n+1/2} \right), \quad S_{j+1/2}^{n+1/2} = S \left( x_{j+1/2}, U_{j+1/2}^{n+1/2} \right), \quad (1.4)$$

and  $U_j^n$  is the average of  $U(x, t_n)$  over the cell  $C_j$  and  $U_{j+1/2}^{n+1/2}$  is the mid-point value or the average of  $U(x_{j+1/2}, t)$  over the time interval  $[t_n, t_{n+1}]$ . The source term  $S(x, U)$  is currently discretized with an interface method, which is the trapezoidal rule in space and the mid-point rule in time [4, 11]. The central issue is how to obtain the mid-point value  $U_{j+1/2}^{n+1/2}$ . The GRP scheme formally approximates this value by the Taylor expansion (ignoring higher order terms),

$$U_{j+1/2}^{n+1/2} \cong U_{j+1/2}^n + \frac{\Delta t}{2} \left( \frac{\partial U}{\partial t} \right)_{j+1/2}^n, \quad (1.5)$$

where

$$U_{j+1/2}^n = \lim_{t \rightarrow t_n+0} U(x_{j+1/2}, t), \quad \left( \frac{\partial U}{\partial t} \right)_{j+1/2}^n = \lim_{t \rightarrow t_n+0} \frac{\partial U}{\partial t}(x_{j+1/2}, t). \quad (1.6)$$

The value  $U_{j+1/2}^n$  is obtained by solving the associated Riemann problem for the homogeneous hyperbolic conservation laws as used in the first-order Godunov scheme [9]. We are left with the calculation of  $(\partial U / \partial t)_{j+1/2}^n$ , which is the main ingredient in the GRP solution.

Let us take a look at a single equation case ( $U, F$  in (1.1) are scalar functions). At each grid point  $(x_{j+1/2}, t_n)$ , only a single wave emanates. Therefore we are able to use the equation (1.1) to get

$$\left( \frac{\partial U}{\partial t} \right)_{j+1/2}^n = -F'(U_{j+1/2}^n) \cdot \left( \frac{\partial U}{\partial x} \right)_{j+1/2}^n + S(x_{j+1/2}, U_{j+1/2}^n), \quad (1.7)$$

where  $(\partial U / \partial x)_{j+1/2}^n$  is upwind taken from the initial data at time  $t = t_n$ . That is,  $(\partial U / \partial x)_{j+1/2}^n$  is taken from the left (resp. right) hand side of  $x = x_{j+1/2}$  if  $F'(U_{j+1/2}^n) > 0$  [resp.  $F'(U_{j+1/2}^n) < 0$ ]. It is clear that the limiting value  $(\partial U / \partial t)_{j+1/2}^n$  does not vanish due to the source term effect even if initially the slopes  $\sigma_j^n$  in (1.2) are identically zero. Therefore even in the first-order Godunov scheme the time derivative  $(\partial U / \partial t)_{j+1/2}^n$  should be properly treated.

In general (1.7) is not valid when (1.1) is a system, because there exists more than one nonlinear wave issuing from the singularity point  $(x_{j+1/2}, t_n)$  and the interface  $x = x_{j+1/2}$  is, generally speaking, located in an intermediate region. We are therefore looking for the substitute of (1.7) in the system case. However, if the system (1.1) is endowed with a coordinate system of Riemann invariants [8, 14], it can be diagonalized and treated as the scalar case. An important and direct consequence is that (1.1) can be transformed into a weakly coupled form, analogous to the linear case mentioned above. Moreover in the associated Riemann problem the Riemann invariants are constant throughout the corresponding rarefaction wave, or in the linearly degenerate case they are continuous across the corresponding contact discontinuity. These properties have the following implications:

- (i) Thinking of the initial data (1.2) with non-zero slopes as a perturbation of piecewise constant Riemann initial data and the source term  $S(x, U)$  as a perturbation of the homogeneous system of equations, the solution of the generalized Riemann problem for (1.1) is a perturbation of the solution of the associated Riemann problem mentioned above at least in the neighborhood of the singularity point. Therefore the Riemann invariants are regular locally across the corresponding (curved) rarefaction wave (in the generalized Riemann problem) although the derivatives of the solution of (1.1) usually explode there. Thus we can take a usual calculus manipulation for the Riemann invariants.
- (ii) Each Riemann invariant is transported with a single equation (see Lemma 6). The transport equation enables us to resolve the rarefaction wave in a quite simple way, analogous to the treatment of the scalar equation. Certainly we need to overcome the technical coupling difficulty by using characteristic coordinates. In this paper, we use the Riemann invariants to resolve the rarefaction waves in the generalized Riemann problem for (1.1) as a main ingredient in our GRP solution.
- (iii) The fact that the Riemann invariants are continuous across the corresponding contact discontinuity simplifies the resolution of contact discontinuities.
- (iv) The existence of Riemann invariants is independent of the Eulerian or Lagrangian formulation of physical models. Therefore, the resulting schemes could be either Eulerian or Lagrangian. We avoid the passage from the Lagrangian version to the Eulerian case, as was done in [1].
- (v) In each rarefaction wave, the behavior of the corresponding Riemann invariant is determined by a suitable (scalar) transport equation. As a consequence, the sonic case, i.e., when the rarefaction wave spans the cell interface, is automatically resolved, see Remarks 12 and 22. Recall that the sonic case is the most delicate in the original GRP scheme [1] or MUSCL-type schemes [10].

Therefore it is natural to use the Riemann invariants to solve the generalized Riemann problem and derive the resulting GRP scheme. This idea has been used in the context of shallow water equations and planar compressible fluid flows [5, 13]. As is well-known [8, Sect. 7.3], any strictly hyperbolic system of two equations is endowed with a coordinate system of Riemann invariants. On the other hand, such a coordinate system does not generally exist for systems of the form (1.1) when  $m \geq 3$ . However, many physical systems are weakly coupled (in a sense to be made precise later, see Definition 21) and can be reduced into a form that is amenable to the Riemann invariant approach. In particular, we can use this approach to handle the system of compressible fluid duct flows in Sect. 7.

Next we point out the difference between our approach and the original GRP scheme [1]. The original GRP scheme was designed for the compressible fluid flows with two related Lagrangian and Eulerian versions. The Eulerian version is always based on the Lagrangian treatment. The transformation is

quite delicate, particularly for sonic cases, because it becomes singular at the sonic point. In contrast, our approach leads to a much simpler direct Eulerian scheme. Another approach by the asymptotic analysis can be found in [7, 15]. We mention here the paper [19] where the GRP is solved assuming the solution is given when the initial data have a general analytic distribution on the two sides of cell interface. We note, however, that our solution to the GRP uses only the limiting values of slopes at the interface and thus it is amenable to any given distributions of flow variables adjacent to the cell interface.

The resulting GRP scheme consists of only two steps: (i) the Riemann solver; (ii) the calculation of  $(\partial U / \partial t)_{j+1/2}^n$ . The (exact or approximate) Riemann solver is standard for many physical systems, see [18] and references therein. The limiting value  $(\partial U / \partial t)_{j+1/2}^n$  is obtained just by solving a linear algebraic system, very close to the linear case of (1.1). This linear system can be obtained either by the analytic GRP for (1.1), in which case we label the GRP method as a  $G_\infty$ -scheme, or by using an acoustic approximation for the GRP, in which case we label the GRP method as a  $G_1$ -scheme. We note that the  $G_1$ -scheme is, in principle, the simplest second-order extension of the Godunov scheme, it just adds about 2–5% computation. We mention also that there are a number of intermediate schemes derived from the analytic resolution. In particular, the  $G_2$ -scheme is actually equivalent to the MUSCL-scheme, see Appendix D in [1].

The structure of the paper is as follows. In Sect. 2, we give the description of the setup of the GRP scheme and the steps for its implementation. In Sect. 3, we discuss the role of Riemann invariants as evolving from classical notions in the case of linear hyperbolic systems. Section 4 treats in detail the case of the system consisting of two equations. This enables us to illustrate clearly the role of Riemann invariants and characteristic coordinates. Then in Sect. 5 we introduce the main topic of the present paper, i.e., the application of the Riemann invariants to general *weakly coupled systems* (WCS). Section 6 is both theoretical and practically important, it introduces an acoustic approximation as the linearized version of nonlinear systems and show how to apply it in the numerical setting. As mentioned above, it leads to a very simple second-order extension of the Godunov scheme. Section 7 is devoted to the discussion of the GRP solution in terms of the abstract method developed in the earlier sections. In particular, in Sect. 7.3 we discuss the system of compressible (non-isentropic) duct flows in the framework of a “weakly coupled system”. In Sect. 8 we give some numerical examples.

## 2 The setup of GRP scheme

The GRP scheme for the numerical approximation of (1.1) assumes piecewise linear initial data in computational cells and relies on analytical solutions of the generalized Riemann problem at each cell interface. For convenience, we set

the cell interface at  $x = 0$  and the initial data as

$$U(x, 0) = \begin{cases} U_L + U'_L x, & x < 0, \\ U_R + U'_R x, & x > 0, \end{cases} \quad (2.1)$$

where  $U_L$ ,  $U_R$ ,  $U'_L$  and  $U'_R$  are constant vectors. We denote by  $U(x, t)$  the solution of (1.1) and (2.1). Correspondingly, the limiting values in (1.6) are denoted by

$$U_* = U(0, 0_+), \quad \left( \frac{\partial U}{\partial t} \right)_* = \frac{\partial U}{\partial t}(0, 0_+). \quad (2.2)$$

The initial structure of the solution  $U(x, t)$  of (1.1) and (2.1) is determined by the associated Riemann problem for

$$\frac{\partial U}{\partial t} + \frac{\partial F(U)}{\partial x} = 0, \quad x \in \mathbb{R}, \quad t > 0, \quad (2.3)$$

subject to the Riemann initial data

$$U(x, 0) = \begin{cases} U_L, & x < 0, \\ U_R, & x > 0. \end{cases} \quad (2.4)$$

We call the solution of (2.3) and (2.4) the *associated Riemann solution* of (1.1) and (2.1). Our GRP scheme is of the Godunov-type and based on the solvability of (2.3) and (2.4).

**Assumption** The Riemann problem (2.3) and (2.4) is uniquely solvable, thus enabling the Godunov scheme.

The Riemann solution of (2.3) and (2.4) is self similar and denoted by  $R^A(x/t; U_L, U_R)$ . Then we have the following proposition [15].

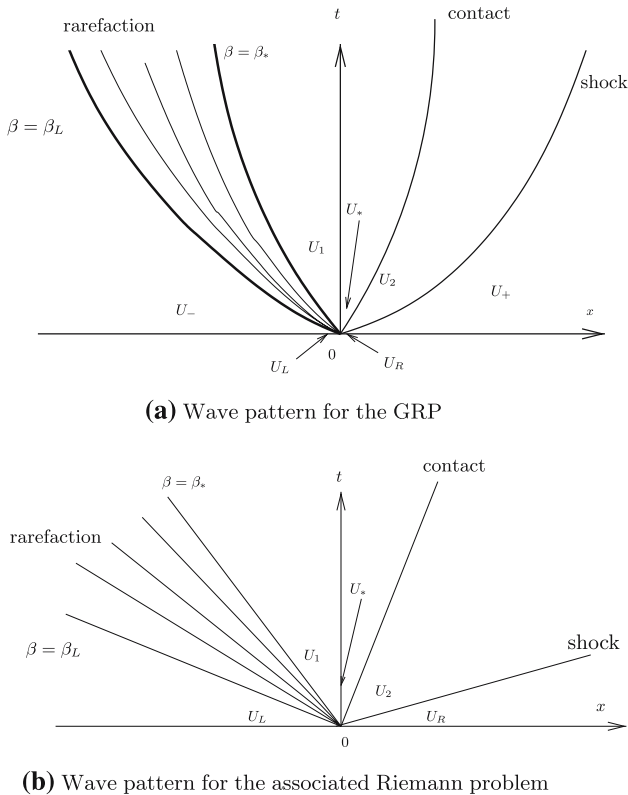
**Proposition 1** *Let  $U(x, t)$  be the solution to the generalized Riemann problem (1.1) and (2.1) and let  $R^A(x/t, U_L, U_R)$  be the solution of the associated Riemann problem (2.3) and (2.4). Then for every fixed direction  $\lambda = x/t$ ,*

$$\lim_{t \rightarrow 0^+} U(\lambda t, t) = R^A(\lambda; U_L, U_R). \quad (2.5)$$

*This implies that the wave configuration for the generalized Riemann problem (1.1) and (2.1) is the same as that for the associated Riemann problem (2.3) and (2.4) near the origin  $(x, t) = (0, 0)$ .*

We illustrate this proposition schematically in Fig. 1. The limiting value  $U_*$  in (2.2) (correspondingly  $U_{j+1/2}^n$  in (1.6)) is just the Riemann solution along the line  $x = 0$ ,

$$U_* = R^A(0; U_L, U_R). \quad (2.6)$$



**Fig. 1** The setup of the GRP scheme

This is already known and used in the Godunov scheme [9]. They can be obtained with the exact or approximate Riemann solver [18]. Therefore, in order to get the GRP scheme, the main issue is only how to calculate  $(\partial U / \partial t)_*$ . Once the limiting value  $(\partial U / \partial t)_*$  is obtained, we implement the GRP scheme by the following four steps.

**Step 1** Given piecewise linear initial data of the type

$$U^n(x) = U_j^n + \sigma_j^n(x - x_j), \quad x \in (x_{j-1/2}, x_{j+1/2}), \quad (2.7)$$

we solve the Riemann problem for (2.3) to define the Riemann solution

$$U_{j+1/2}^n = R^A \left( 0; U_j^n + \frac{\Delta x}{2} \sigma_j^n, U_{j+1}^n - \frac{\Delta x}{2} \sigma_{j+1}^n \right). \quad (2.8)$$

This is the same as the classical Godunov scheme [9].

**Step 2** Determine  $(\partial U / \partial t)_{j+1/2}^n$ . This is the main theme in the present paper. It turns out that this time derivative of solution vector is obtained by simply solving a linear algebraic system of equations.

**Step 3** Approximate numerically the solution of (1.1) by using (1.3) and (1.5).

**Step 4** Update the slope by the following procedure. Define

$$\begin{aligned} U_{j+1/2}^{n+1,-} &= U_{j+1/2}^n + \Delta t \left( \frac{\partial U}{\partial t} \right)_{j+1/2}^n, \\ \sigma_j^{n+1,-} &= \frac{1}{\Delta x} (\Delta U)_j^{n+1,-} = \frac{1}{\Delta x} \left( U_{j+1/2}^{n+1,-} - U_{j-1/2}^{n+1,-} \right). \end{aligned} \quad (2.9)$$

Then in order to suppress oscillations near discontinuities we modify  $\sigma_j^{n+1,-}$  by a monotonicity algorithm to get  $\sigma_j^{n+1}$ , see [1, 12, 17], in the sense of slope limiters. For the numerical examples in Sect. 8, we use the following limiter

$$\sigma_j^{n+1} = \text{minmod} \left( \alpha \frac{U_j^{n+1} - U_{j-1}^{n+1}}{\Delta x}, \sigma_j^{n+1,-}, \alpha \frac{U_{j+1}^{n+1} - U_j^{n+1}}{\Delta x} \right), \quad (2.10)$$

where the parameter  $\alpha \in [0, 2)$ .

**Remark 2** (Stationary discontinuity) In the case of a stationary discontinuity which is expressed by  $x = x(t)$ ,  $x'(0) = 0$ , the value  $U_*$  in (2.2) is double-valued. Denote  $U_{\pm} = R^A(0 \pm 0; U_L, U_R)$ . Then we have  $F(U_-) = F(U_+)$ , which justifies the fact that either of  $U_{\pm}$  can be used in the Godunov scheme. In the GRP scheme, we need further to detect the initial curvature of the discontinuity, i.e., the sign of  $x''(0)$ .

### 3 Heuristic explanation from a linear system

In this section we use a familiar linear system to explain the necessity to introduce the Riemann invariants in upwind (the Godunov-type) schemes. The linear example is

$$\frac{\partial u}{\partial t} + c \frac{\partial v}{\partial x} = 0, \quad \frac{\partial v}{\partial t} + c \frac{\partial u}{\partial x} = 0, \quad (3.1)$$

where  $c > 0$  is constant. This model describes two linear waves: One propagates to the left with velocity  $-c$  and the other to the right with velocity  $c$ .

For the given initial data of type (2.1), where  $U = (u, v)^{\top}$ , the solution is discontinuous at the origin and the discontinuities propagate along characteristics. Therefore we are not able to use (3.1) to simply get  $\partial u / \partial t$  and  $\partial v / \partial t$ , as in the single equation case. However, if (3.1) is written in the following form

$$\frac{\partial(u-v)}{\partial t} - c \frac{\partial(u-v)}{\partial x} = 0, \quad \frac{\partial(u+v)}{\partial t} + c \frac{\partial(u+v)}{\partial x} = 0, \quad (3.2)$$

we see that the function  $u + v$  (resp.  $u - v$ ) is smooth on the two sides of the characteristic  $dx/dt = c$  (resp.  $dx/dt = -c$ ). The functions  $u \pm v$  correspond to the Riemann invariants in nonlinear cases. Turning back to the system (3.1),



we denote  $u'_* = \lim_{t \rightarrow 0^+} (\partial u / \partial x)(0, t)$  (similarly for  $v'_*$ ). Then we can proceed, as in scalar cases, to get

$$\begin{aligned} u_* + v_* &= u_L + v_L, & u'_* + v'_* &= u'_L + v'_L, & u_* - v_* &= u_R - v_R, \\ u'_* - v'_* &= u'_R - v'_R. \end{aligned} \quad (3.3)$$

By using (3.2), we have

$$\left( \frac{\partial u}{\partial t} \right)_* + \left( \frac{\partial v}{\partial t} \right)_* = -c(u'_L + v'_L), \quad \left( \frac{\partial u}{\partial t} \right)_* - \left( \frac{\partial v}{\partial t} \right)_* = c(u'_R - v'_R). \quad (3.4)$$

In order to get  $(\partial u / \partial t)_*$  and  $(\partial v / \partial t)_*$ , we need to solve (3.4) and get

$$\left( \frac{\partial u}{\partial t} \right)_* = -\frac{c(u'_L + v'_L)}{2} + \frac{c(u'_R - v'_R)}{2}, \quad \left( \frac{\partial v}{\partial t} \right)_* = -\frac{c(u'_L + v'_L)}{2} - \frac{c(u'_R - v'_R)}{2}. \quad (3.5)$$

This is essentially the solution of GRP for (3.1).

We summarize the above process in the following two steps:

- (i) Find Riemann invariants and obtain their time derivatives. Thus the system of linear equations (3.4) is derived.
- (ii) Solve the resulting linear system of algebraic equations to yield the limiting values  $(\partial u / \partial t)_*$  and  $(\partial v / \partial t)_*$ .

In the nonlinear case of (1.1), we also perform these two steps. In particular, the concept of Riemann invariants plays a pivotal role and corresponds to the quantities  $u + v$  and  $u - v$  here. They are used to analytically resolve the rarefaction waves in the generalized Riemann problem (1.1) and (2.1), which constitutes the important feature of the resulting scheme. In addition, they are useful in resolving contact discontinuities.

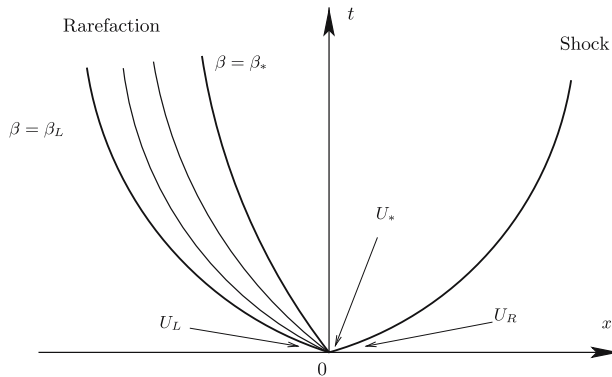
#### 4 The resolution of generalized Riemann problem for the two-equation system

In this section we focus on the case of a strictly hyperbolic system of two equations. We note that the physical models of isentropic (compressible) flows and shallow water equations are examples of such systems. Furthermore, we shall later show that the main idea here carries over to a broader class of general systems.

Thus, we assume that (1.1) consists of two equations and denote  $U = (u, v)^\top$  and  $F = (f(u, v), g(u, v))^\top$ . The Jacobian matrix  $DF(U) = \partial F / \partial U$  has two distinct eigenvalues

$$\lambda(u, v) < \mu(u, v), \quad (4.1)$$

and further assume that  $\lambda$  and  $\mu$  are genuinely nonlinear, and thus their associated waves are either a rarefaction wave or a shock [8, 16]. We consider the typical wave pattern, as shown in Fig. 2. The result is stated in the following theorem. The proof of Theorem is given in Sects. 4.1 and 4.2.



**Fig. 2** A typical wave pattern for the two-equation case

**Theorem 3** Assume that the local wave pattern for the generalized Riemann problem (1.1) is as depicted in Fig. 2, and the  $t$ -axis is inside the intermediate (smooth) region. Then the limiting value  $(\partial U / \partial t)_*$  can be obtained by solving the following pair of linear algebraic equations,

$$\begin{cases} a_L \left( \frac{\partial u}{\partial t} \right)_* + b_L \left( \frac{\partial v}{\partial t} \right)_* = d_L, \\ a_R \left( \frac{\partial u}{\partial t} \right)_* + b_R \left( \frac{\partial v}{\partial t} \right)_* = d_R, \end{cases} \quad (4.2)$$

where  $a_L$ ,  $b_L$  and  $d_L$  are given in Lemma 7 and  $a_R$ ,  $b_R$  and  $d_R$  are given in Lemma 10.

#### 4.1 The resolution of rarefaction waves for two-equation system

As in [8, Sect. 7.3] the system is endowed with a coordinate system of Riemann invariants which we shall denote by  $\phi$  and  $\psi$ . In terms of these new unknowns (1.1) is reduced into the form

$$\begin{cases} \frac{\partial \phi}{\partial t} + \lambda(\phi, \psi) \frac{\partial \phi}{\partial x} = k_1(x, \phi, \psi), \\ \frac{\partial \psi}{\partial t} + \mu(\phi, \psi) \frac{\partial \psi}{\partial x} = k_2(x, \phi, \psi), \end{cases} \quad (4.3)$$

where  $k_1$  and  $k_2$  are two functions resulting from the source term of (1.1) and they are expressed in terms of the Riemann invariants  $\phi$ ,  $\psi$ . For uniformity, we denote  $W = (\phi, \psi)^\top$ ,  $K = (k_1, k_2)^\top$  and  $\Lambda = \text{diag}(\lambda, \mu)$ . Then (4.3) is rewritten as

$$\frac{\partial W}{\partial t} + \Lambda(W) \frac{\partial W}{\partial x} = K(x, W). \quad (4.4)$$

As pointed out earlier, the main feature of the GRP scheme is the resolution of rarefaction waves. In this context, it will turn out that the concept of characteristic coordinates is quite useful.

#### 4.1.1 Characteristic coordinates

The characteristic coordinates, as the integral curves of characteristic equations, play an important role in the resolution of rarefaction waves and simplify the calculation. Let  $C^\lambda : \beta(x, t) = \text{const.}$  be the integral curve of the differential equation

$$\frac{dx}{dt} = \lambda(\phi, \psi), \quad (4.5)$$

and  $C^\mu : \alpha(x, t) = \text{const.}$  be the integral curve of the differential equation

$$\frac{dx}{dt} = \mu(\phi, \psi). \quad (4.6)$$

Consider a domain in the  $(x, t)$ -plane where the coordinates  $(x, t)$  can be obtained as functions of  $\alpha$  and  $\beta$ . This transformation is denoted by

$$t = t(\alpha, \beta), \quad x = x(\alpha, \beta). \quad (4.7)$$

In terms of the characteristic coordinates  $(\alpha, \beta)$ , the system (4.3) can be rewritten in the form of the characteristic equations

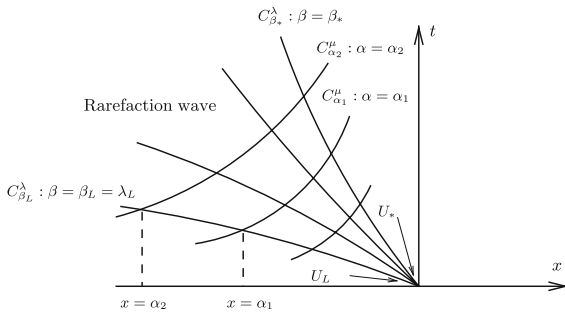
$$\begin{cases} \frac{\partial x}{\partial \alpha} = \lambda(\phi, \psi) \frac{\partial t}{\partial \alpha}, & \frac{\partial \phi}{\partial \alpha} = \frac{\partial t}{\partial \alpha} \cdot k_1(x(\alpha, \beta), \phi, \psi), \\ \frac{\partial x}{\partial \beta} = \mu(\phi, \psi) \frac{\partial t}{\partial \beta}, & \frac{\partial \psi}{\partial \beta} = \frac{\partial t}{\partial \beta} \cdot k_2(x(\alpha, \beta), \phi, \psi). \end{cases} \quad (4.8)$$

It follows, by differentiating the first pair of equations with respect to  $\beta$ , the second with respect to  $\alpha$  and subtracting, that  $t = t(\alpha, \beta)$  satisfies,

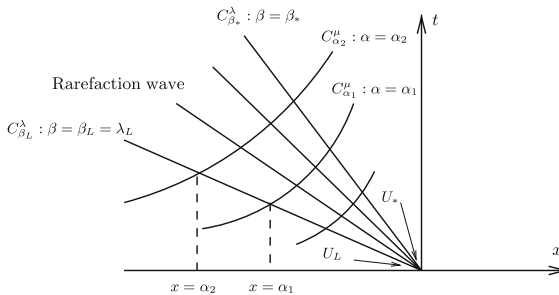
$$(\lambda - \mu) \frac{\partial^2 t}{\partial \alpha \partial \beta} + \frac{\partial \lambda}{\partial \beta} \frac{\partial t}{\partial \alpha} - \frac{\partial \mu}{\partial \alpha} \frac{\partial t}{\partial \beta} = 0. \quad (4.9)$$

We differentiate the  $\psi$ -equation in (4.8) with respect to  $\alpha$  and incorporate (4.9) into the resulting equation to get that  $\psi = \psi(\alpha, \beta)$  satisfies

$$\begin{aligned} \frac{\partial^2 \psi}{\partial \alpha \partial \beta} &= \frac{\partial^2 t}{\partial \alpha \partial \beta} \cdot k_2(x(\alpha, \beta), \phi, \psi) + \frac{\partial t}{\partial \beta} \frac{\partial k_2}{\partial \alpha} \\ &= -\frac{k_2}{\lambda - \mu} \cdot \frac{\partial \lambda}{\partial \beta} \cdot \frac{\partial t}{\partial \alpha} + \frac{\partial t}{\partial \beta} \left( \frac{k_2}{\lambda - \mu} \frac{\partial \mu}{\partial \alpha} + \frac{\partial k_2}{\partial \alpha} \right). \end{aligned} \quad (4.10)$$



(a) The curved rarefaction wave in the generalized Riemann problem



(b) The rarefaction wave in the associated Riemann problem

**Fig. 3** Characteristic coordinates throughout a centered rarefaction wave

Similarly, we have the second-order equation for the Riemann invariant  $\phi$ ,

$$\frac{\partial^2 \phi}{\partial \alpha \partial \beta} = -\frac{k_1}{\mu - \lambda} \cdot \frac{\partial \mu}{\partial \alpha} \cdot \frac{\partial t}{\partial \beta} + \frac{\partial t}{\partial \alpha} \left( \frac{k_1}{\mu - \lambda} \frac{\partial \lambda}{\partial \beta} + \frac{\partial k_1}{\partial \beta} \right). \quad (4.11)$$

Next we turn to the detailed analysis of the rarefaction wave for the generalized Riemann problem (1.1) and (2.1). In view of Proposition 1, when approaching the origin  $(x, t) = (0, 0)$ , the solution  $U(x, t)$  is determined by the associated Riemann solution  $R^A(x/t; U_L, U_R)$ . We can therefore regard the former as a perturbation of the latter. When investigating the (curved) centered rarefaction wave for the generalized Riemann problem, we will use the same domain of characteristic coordinates as the one determined by the associated rarefaction wave.

#### 4.1.2 The resolution of rarefaction waves

We start with the rarefaction wave for the associated Riemann problem (2.3) and (2.4). We assume the structure as in Fig. 3b and the rarefaction wave is denoted by  $R_\lambda^A$ . Further, the  $t$ -axis is located in the smooth domain behind the rarefaction wave  $R_\lambda^A$ .

Since  $\psi$  is constant across the rarefaction wave  $R_\lambda^A$ , we express it by using

$$\begin{cases} \lambda(\phi, \psi) = x/t, \\ \psi = \psi_L, \end{cases} \quad (4.12)$$

where  $\psi_L$  is the value of  $\psi$  at the head characteristic of  $R_\lambda^A$ , i.e.,  $\beta = \beta_L$ . This rarefaction wave expands from  $\beta_L$  up to  $\beta_*$ . In this case, Eq. (4.5) gives us simply  $\beta = x/t$ . The characteristic coordinate  $\alpha$  is found as follows. In view of (4.12), one has  $\lambda(\phi, \psi_L) = \beta$ , which can be inverted to yield, by using the property of genuine nonlinearity of  $\lambda$ ,

$$\phi = \phi(x/t; \psi_L) = \phi(\beta; \psi_L). \quad (4.13)$$

Then the characteristic curve  $C_{\alpha_0}^\mu : \alpha(x, t) = \alpha_0$  is the integral curve of the equation

$$\frac{dx}{dt} = \mu(\phi, \psi) = \mu(\phi(x/t; \psi_L), \psi_L), \quad (4.14)$$

where the constant  $\alpha_0$  is chosen to be the  $x$ -coordinate of the intersection point of  $C_{\alpha_0}^\mu$  with the leading  $\lambda$ -characteristic curve  $C_{\beta_L}^\lambda$ . This determines  $(x, t)$  as functions of  $(\alpha, \beta)$ .

Denote the corresponding characteristic map to the  $(x, t)$ -plane by

$$t = t_{\text{ass}}(\alpha, \beta), \quad x = x_{\text{ass}}(\alpha, \beta). \quad (4.15)$$

All other variables including the eigenvalues  $\lambda$ ,  $\mu$  and Riemann invariants can now be expressed as smooth functions of  $(\alpha, \beta)$ . We observe that the characteristic map is singular at  $\alpha = 0$ , where the segment between  $\beta_L$  and  $\beta_*$  is mapped to the origin  $(x, t) = (0, 0)$ . We note that  $t_{\text{ass}}(\alpha = 0, \beta) \equiv 0$  and thus  $(\partial t_{\text{ass}}/\partial \beta)(0, \beta) = 0$ . Then in view of (4.9) we have

$$(\lambda - \mu) \frac{\partial^2 t_{\text{ass}}}{\partial \alpha \partial \beta}(0, \beta) = -\frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta) \cdot \frac{\partial \lambda}{\partial \beta}(0, \beta). \quad (4.16)$$

Since  $(\partial \lambda/\partial \beta)(0, \beta) = 1$ , by the definition of  $\beta$ -coordinate, we get

$$\frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta) = \frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta_L) \exp \left( \int_{\beta_L}^{\beta} \frac{1}{(\mu - \lambda)(0, \xi)} d\xi \right). \quad (4.17)$$

By our choice of the  $\alpha$ -coordinate as the  $x$ -value of the intersection point of  $C_\alpha^\mu$  with the leading characteristic  $C_{\beta_L}^\lambda$ , we obtain  $(\partial x_{\text{ass}}/\partial \alpha)(0, \beta_L) = 1$ . Then we use (4.8) to get

$$\frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta_L) = \frac{1}{\beta_L} \frac{\partial x_{\text{ass}}}{\partial \alpha}(0, \beta_L) = \frac{1}{\beta_L}. \quad (4.18)$$

This together with (4.17) gives the explicit expressions for the derivatives of  $t_{\text{ass}}(\alpha, \beta)$ ,  $x_{\text{ass}}(\alpha, \beta)$  at the singularity point  $(x, t) = (0, 0)$ ,

$$\begin{aligned} \frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta) &= \frac{1}{\beta_L} \exp \left( \int_{\beta_L}^{\beta} \frac{1}{\mu(0, \xi) - \xi} d\xi \right), \quad \frac{\partial x_{\text{ass}}}{\partial \alpha}(0, \beta) \\ &= \frac{\beta}{\beta_L} \exp \left( \int_{\beta_L}^{\beta} \frac{1}{\mu(0, \xi) - \xi} d\xi \right). \end{aligned} \quad (4.19)$$

**Remark 4** Inspecting (4.12), (4.13) and (4.17), we see that the ratio between  $(\partial t_{\text{ass}}/\partial \alpha)(0, \beta)$  and  $(\partial t_{\text{ass}}/\partial \alpha)(0, \beta_L)$  is function of  $\beta$  and is independent of the  $\alpha$ -coordinate. Therefore, we retain the degree of freedom in our choice of  $\alpha$ , which will simplify some calculation, see Sect. 7.

In the following we turn to deal with the generalized Riemann problem (1.1) and (2.1), and consider the general (curved) rarefaction wave, see Fig. 3a. The characteristic curves inside the curved rarefaction wave  $t = t(\alpha, \beta)$ ,  $x = x(\alpha, \beta)$  are second-order approximations of  $t_{\text{ass}}(\alpha, \beta)$  and  $x_{\text{ass}}(\alpha, \beta)$  as  $\alpha \rightarrow 0$ . This fact is stated in the following proposition and the proof (which we omit) follows the same lines as in [4, Chap. 5].

**Proposition 5** *As  $\alpha \rightarrow 0$ , we have the following asymptotic expressions for  $t(\alpha, \beta)$ ,  $x(\alpha, \beta)$ ,*

$$t(\alpha, \beta) = t_{\text{ass}}(\alpha, \beta) + O(\alpha^2), \quad x(\alpha, \beta) = x_{\text{ass}}(\alpha, \beta) + O(\alpha^2), \quad (4.20)$$

where  $\beta_L \leq \beta \leq \beta_*$ .

With this proposition, we have the following lemmas about the resolution of the rarefaction wave.

**Lemma 6** *Let  $\psi_\alpha(0, \beta) = \frac{\partial \psi}{\partial \alpha}(0, \beta)$  and denote  $k_{2,L} = k_2(0, \phi_L, \psi_L)$  (see the RHS of (4.3)). Then throughout the rarefaction wave associated with  $\lambda$ , we have*

$$\psi_\alpha(0, \beta) = \psi_\alpha(0, \beta_L) + \int_{\beta_L}^{\beta} -\frac{k_2}{\lambda - \mu}(0, \xi) \cdot \frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \xi) d\xi, \quad \beta_L \leq \beta \leq \beta_*. \quad (4.21)$$

The initial datum  $\psi_\alpha(0, \beta_L)$  is

$$\psi_\alpha(0, \beta_L) = \psi'_L + \frac{1}{\beta_L} (k_{2,L} - \mu_L \psi'_L), \quad (4.22)$$

where  $\psi'_L$  is determined by  $U_L$ ,  $U'_L$  as in (2.1).

*Proof* Recall that

$$\frac{\partial t(0, \beta)}{\partial \beta} = 0, \quad \frac{\partial x(0, \beta)}{\partial \beta} = 0. \quad (4.23)$$

The asymptotic behavior of solutions at the origin, see Proposition 5, shows

$$\frac{\partial t}{\partial \alpha}(0, \beta) = \frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta), \quad \frac{\partial x}{\partial \alpha}(0, \beta) = \frac{\partial x_{\text{ass}}}{\partial \alpha}(0, \beta). \quad (4.24)$$

Therefore, setting  $\alpha = 0$  in (4.10), we obtain

$$\frac{\partial}{\partial \beta}(\psi_\alpha(0, \beta)) = -\frac{k_2}{\lambda - \mu}(0, \beta) \cdot \frac{\partial t_{\text{ass}}}{\partial \alpha}(0, \beta), \quad \beta \in (\beta_L, \beta_*), \quad (4.25)$$

which yields (4.21) by integration.

The initial datum  $\psi_\alpha(0, \beta_L)$  comes from the characteristic form (4.8) by using the chain rule,

$$\begin{aligned} \frac{\partial \psi}{\partial \alpha}(0, \beta_L) &= \frac{\partial \psi}{\partial x}(0, \beta_L) \frac{\partial x}{\partial \alpha}(0, \beta_L) + \frac{\partial \psi}{\partial t}(0, \beta_L) \frac{\partial t}{\partial \alpha}(0, \beta_L) \\ &= \psi'_L + \frac{\partial \psi}{\partial t}(0, \beta_L) \cdot \frac{1}{\beta_L}, \end{aligned} \quad (4.26)$$

where we use the fact that  $(\partial x / \partial \alpha)(0, \beta_L) = 1$  and  $(\partial t / \partial \alpha)(0, \beta_L) = 1 / \beta_L$ . Then we use the  $\psi$ -equation in (4.3) to get (4.22).

**Lemma 7** Consider the rarefaction wave  $R_\lambda$  associated with  $\lambda$ . Then we have

$$a_L \left( \frac{\partial u}{\partial t} \right)_* + b_L \left( \frac{\partial v}{\partial t} \right)_* = d_L^*, \quad (4.27)$$

where  $(a_L, b_L) = (\nabla_U \psi)_*$ ,  $\nabla_U \psi = (\partial \psi / \partial u, \partial \psi / \partial v)$  and

$$d_L^* = \frac{\mu_*}{\mu_* - \lambda_*} \cdot \left( \psi_\alpha(0, \beta_*) \cdot \left( \frac{\partial t_{\text{ass}}}{\partial \alpha} \right)^{-1}(0, \beta_*) - \frac{\lambda_*}{\mu_*} \cdot k_2(0, \phi_*, \psi_*) \right). \quad (4.28)$$

*Proof* We use the result of Lemma 6 at  $\beta = \beta_*$  and express the directional derivative in terms of  $(x, t)$  derivatives. Using the equations for  $\psi$  in (4.8) and (4.3), one obtains,

$$\begin{aligned} \psi_\alpha(0, \beta_*) &= \frac{\partial t_{\text{ass}}(0, \beta_*)}{\partial \alpha} \cdot \left( \frac{\partial \psi}{\partial t} + \lambda \frac{\partial \psi}{\partial x} \right)(0, \beta_*) \\ &= \frac{\partial t_{\text{ass}}(0, \beta_*)}{\partial \alpha} \left[ \left( \frac{\partial \psi}{\partial t} \right)_* + \frac{\lambda_*}{\mu_*} \left( - \left( \frac{\partial \psi}{\partial t} \right)_* + k_2(0, \phi_*, \psi_*) \right) \right]. \end{aligned} \quad (4.29)$$

It follows that,

$$\left(\frac{\partial \psi}{\partial t}\right)_* = \frac{\mu_*}{\mu_* - \lambda_*} \cdot \left[ \psi_\alpha(0, \beta_*) \cdot \left(\frac{\partial t_{\text{ass}}}{\partial \alpha}\right)^{-1}(0, \beta_*) - \frac{\lambda_*}{\mu_*} \cdot k_2(0, \phi_*, \psi_*) \right], \quad (4.30)$$

where  $\lambda_* = \beta_*$ . We note that  $\psi$  is regular across the characteristic  $C_{\beta_*}^\lambda$ . Hence the value of  $\psi_\alpha(0, \beta_*)$  can be evaluated using the values of  $\partial \psi / \partial t$ ,  $\partial \psi / \partial x$  in the smooth domain behind the rarefaction wave  $R_\lambda$ . We write  $\psi$  in terms of  $U$  and immediately arrive at (4.27).

*Remark 8* Note that the term  $\psi_\alpha(0, \beta_*) \cdot \left(\frac{\partial t_{\text{ass}}}{\partial \alpha}\right)^{-1}(0, \beta_*)$  is clearly independent of the choice of  $\alpha$ , cf. Remark 4.

*Remark 9* One might wonder why we use  $\psi$ , rather than  $\phi$ , in resolving  $R_\lambda^A$ . The reason is that on one hand,  $\psi$  is constant throughout  $R_\lambda^A$  in the associated Riemann solution,  $\psi$  is still regular even when the initial data has non-zero slopes and the source term is present in the governing equation (4.3). On the other hand,  $\phi_\alpha(0, \beta_*) = k_1(0, \phi_*, \psi_*) \cdot (\partial t_{\text{ass}} / \partial \alpha)(0, \beta_*)$  and we cannot express  $(\partial \phi / \partial t)_*$  in terms of  $\phi_\alpha$  since there is no equivalent equation to Eq. (4.29).

## 4.2 The resolution of shocks for the two-equation system

We assume that the wave associated with the  $\mu$  family is a shock moving to the right and let the shock trajectory be  $x = x(t)$  with the speed  $\sigma(t) = x'(t)$ , separating two limiting states  $U$ ,  $\bar{U}$ . To fix the ideas, we assume that  $\bar{U}$  is the state ahead of the shock while  $U$  is the state behind it. This shock is described by the Rankine–Hugoniot jump condition,

$$F(U) - F(\bar{U}) = \sigma(U - \bar{U}). \quad (4.31)$$

Then we know [8, Sect. 8.2] that if a state  $U$  connects to  $\bar{U}$  by the shock with speed  $\sigma$ , (4.31) gives the Hugoniot locus of the form,

$$\begin{cases} \sigma = \sigma(U, \bar{U}), \\ U = \bar{U} + \tau K(U, \bar{U}), \end{cases} \quad (4.32)$$

where  $\tau > 0$  is a parameter describing the strength of the shock. In fact, the system (4.32) corresponds to one of the two shock curves associated with  $\lambda$ ,  $\mu$  (recall that  $\lambda$ ,  $\mu$  are two genuinely nonlinear eigenvalues for the system of two equations in Sect. 4.1). Eliminating the parameter  $\tau$  from (4.32) yields a single equation connecting the state  $\bar{U} = (\bar{u}, \bar{v})$  to the state  $U = (u, v)$ , given by

$$\Psi(U; \bar{U}) = 0. \quad (4.33)$$



This is indeed the equation for the Hugoniot curve in the state  $(u, v)$ -plane, and it holds along the shock trajectory  $x = x(t)$  identically. Note that  $U, \bar{U}$  are the limiting states on both sides of  $x = x(t)$ ,  $U = U(x(t), t)$ ,  $\bar{U} = \bar{U}(x(t), t)$ , where we are now using  $U$  and  $\bar{U}$  also for the full states behind and ahead of the shock, respectively.

In terms of Riemann invariants  $W$  (see (4.4) for the notation  $W$ ), we can rewrite (4.33) in the form

$$\Phi(W; \bar{W}) = 0. \quad (4.34)$$

We may therefore differentiate (4.34) in the direction of the shock  $x = x(t)$  and get

$$\nabla_W \Phi \left( \frac{\partial W}{\partial t} + \sigma \frac{\partial W}{\partial x} \right) = -\nabla_{\bar{W}} \Phi \left( \frac{\partial \bar{W}}{\partial t} + \sigma \frac{\partial \bar{W}}{\partial x} \right). \quad (4.35)$$

We want to solve (4.35) for  $\partial W / \partial t$ . We are assuming that the  $t$ -axis is located in the intermediate region so that  $\lambda < 0$  and  $\mu > 0$  (see Fig. 2). In the sonic case where the  $t$ -axis is located in the rarefaction wave, we already have the full solution, see Sect. 12 below. We use the diagonal form (4.4) to obtain,

$$\frac{\partial W}{\partial x} = \Lambda(W)^{-1} \left( -\frac{\partial W}{\partial t} + K(x, W) \right), \quad \frac{\partial \bar{W}}{\partial t} = -\Lambda(\bar{W}) \frac{\partial \bar{W}}{\partial x} + K(x, \bar{W}). \quad (4.36)$$

Note that the limiting values of  $\sigma$ ,  $W$ ,  $\bar{W}$ ,  $\partial W / \partial t$  and  $\partial \bar{W} / \partial x$  (see Eqs. (2.1), (2.2)) are

$$\begin{aligned} \lim_{t \rightarrow 0^+} \sigma &= \sigma_0, \quad \lim_{t \rightarrow 0^+} W = W_*, \quad \lim_{t \rightarrow 0^+} \frac{\partial W}{\partial t} = \left( \frac{\partial W}{\partial t} \right)_*, \\ \lim_{t \rightarrow 0^+} \bar{W} &= W_R, \quad \lim_{t \rightarrow 0^+} \frac{\partial \bar{W}}{\partial x} = W'_R, \end{aligned} \quad (4.37)$$

where the limits in (4.37) correspond to our assumption that  $\sigma_0 > 0$ , so that the shock moves into the domain  $x > 0$ , leaving the  $t$ -axis in the smooth domain behind it. It is clear how to change the limits when  $\sigma_0 < 0$ . Then we use (4.36), (4.37) in (4.35) so as to obtain

$$\begin{aligned} &\nabla_W \Phi(W_*; W_R) (I - \sigma_0 \Lambda(W_*)^{-1}) \left( \frac{\partial W}{\partial t} \right)_* \\ &= -\sigma_0 \nabla_W \Phi(W_*; W_R) \Lambda(W_*)^{-1} K(0, W_*) \\ &\quad - \nabla_{\bar{W}} \Phi(W_*; W_R) [(\sigma_0 I - \Lambda(W_R)) W'_R + K(0, W_R)]. \end{aligned} \quad (4.38)$$

We express  $\partial W / \partial t$  in terms of  $\partial U / \partial t$  (as in the end of the proof of Theorem 7), in order to obtain the following lemma.

**Lemma 10** Consider the two equation system (1.1), subject to the initial data (2.1). Assume that the wave pattern is as in Fig. 2, i.e., the wave associated with the  $\mu$  family is a shock moving to the right and that the  $t$ -axis is contained in the smooth region behind it. Then the two components of  $(\partial U/\partial t)_*$  (see (2.2)) satisfy the following linear equation at the singularity  $(x, t) = (0, 0)$ ,

$$a_R \left( \frac{\partial u}{\partial t} \right)_* + b_R \left( \frac{\partial v}{\partial t} \right)_* = d_R, \quad (4.39)$$

where the coefficients  $a_R$ ,  $b_R$  and  $d_R$  are given explicitly as

$$\begin{aligned} (a_R, b_R) &= \nabla_W \Phi(W_*; W_R) (I - \sigma_0 \Lambda(W_*)^{-1}) DW(U_*), \\ d_R &= -\sigma_0 \nabla_W \Phi(W_*; W_R) \Lambda(W_*)^{-1} K(0, W_*) \\ &\quad - \nabla_{\bar{W}} \Phi(W_*; W_R) [(\sigma_0 I - \Lambda(U_R)) W'_R + K(0, W_R)]. \end{aligned} \quad (4.40)$$

**Remark 11** If the eigenvalue  $\mu$  is linearly degenerate, the corresponding jump discontinuity is a contact discontinuity. For this case,  $\sigma(W, \bar{W}) = \mu(W) = \mu(\bar{W})$  and in the limit

$$I - \sigma_0 \Lambda(W_*)^{-1} = \begin{pmatrix} (\lambda_* - \mu_*)/\lambda_* & 0 \\ 0 & 0 \end{pmatrix}, \quad \sigma_0 I - \Lambda(W_R) = \begin{pmatrix} \mu_R - \lambda_R & 0 \\ 0 & 0 \end{pmatrix}, \quad (4.41)$$

The first component of equation (4.38) gives a scalar equation

$$\begin{aligned} &\frac{\partial \Phi(W_*; W_R)}{\partial \phi} \cdot \frac{\lambda_* - \mu_*}{\lambda_*} \cdot \left( \frac{\partial \phi}{\partial t} \right)_* \\ &= -\mu_* \nabla_W \Phi(W_*; W_R) \Lambda(W_*)^{-1} K(0, W_*) \\ &\quad - \frac{\partial \Phi(W_*; W_R)}{\partial \phi} \cdot (\mu_R - \lambda_R) \cdot (\phi'_R + k_1(0, W_R)). \end{aligned} \quad (4.42)$$

These arguments also apply to the acoustic case that will be discussed later on. The idea will be used to consider weak shocks as characteristic curves, thus treating the weak shocks as linearly degenerate discontinuities. Clearly we can also obtain a linear equation in the same form as (4.39) with coefficients

$$\begin{aligned} (a_R, b_R) &= \frac{\partial \Phi(W_*; W_R)}{\partial \phi} \cdot \frac{\lambda_* - \mu_*}{\lambda_*} \cdot (\nabla_U \phi)_*, \\ d_R &= -\mu_* \nabla_W \Phi(W_*; W_R) \Lambda(W_*)^{-1} K(0, W_*) \\ &\quad - \frac{\partial \Phi(W_*; W_R)}{\partial \phi} \cdot (\mu_R - \lambda_R) \cdot (\phi'_R + k_1(0, W_R)). \end{aligned} \quad (4.43)$$

**Remark 12** (The sonic case) Special attention should be paid to the case where the  $t$ -axis (the cell interface  $x = 0$ ) is contained in the rarefaction wave, so that it

is tangential to one of The characteristic curves. We refer to this case as a *sonic case*. Then we have to modify the above approach. Indeed, it becomes much simpler. We still use the notations in Sect. 4. Consider the rarefaction wave associated with  $\lambda$ . We see that the equation (4.27) for  $\psi$  is still valid, where  $\beta_*$  is replaced by  $\beta_0 = 0$ . In addition, let  $C_{\beta_0}^\lambda$  be the characteristic curve tangent to the  $t$ -axis,  $\beta_L < \beta_0 = 0 < \beta_*$ , so that we have  $\lambda(\phi_0, \psi_0) = 0$ . Then we obtain from (4.8), with  $\beta_* = \beta_0$ ,

$$\phi_\alpha(0, \beta_*) = k_1(0, \phi_*, \psi_*) \cdot (\partial t_{ass}/\partial \alpha)(0, \beta_*) \quad (4.44)$$

That is,

$$(\nabla_U \phi)_0 \left( \frac{\partial U}{\partial t} \right)_* = k_1(0, \phi_0, \psi_0). \quad (4.45)$$

We therefore obtain in this case the following theorem.

**Theorem 13** (Sonic case) *Assume that the  $t$ -axis is located inside the rarefaction wave associated with  $\lambda$ . Then we can calculate the limiting values of the time derivatives  $(\partial U/\partial t)_*$  by solving the following system of two linear algebraic equations,*

$$\begin{aligned} (\nabla_U \psi)_0 \left( \frac{\partial U}{\partial t} \right)_* &= d_L^0, \\ (\nabla_U \phi)_0 \left( \frac{\partial U}{\partial t} \right)_* &= k_1(0, \phi_0, \psi_0), \end{aligned} \quad (4.46)$$

where  $d_L^0 = d_L^*(0, \beta = 0)$ ,  $d_L^*$  is defined in (4.28). Note that  $\lambda_* = 0$  for the present case. Then  $d_L^0 = \psi_\alpha(0, 0) \cdot (\partial t_{ass}/\partial \alpha)^{-1}(0, 0)$  (see Eq. (4.19) with  $\beta = 0$  for  $(\partial t_{ass}/\partial \alpha)(0, \beta)$ ).

**Remark 14** (Stationary shock) When the shock trajectory  $x = x(t)$  is tangent to the  $t$ -axis,  $x'(0) = 0$ , we need to just the sign of  $x''(0)$ , as pointed out in Remark 2. Denote  $U_\pm(t) = U(x(t) \pm 0, t)$ . Then we have

$$x''(0)(U_+ - U_-) = \frac{\partial F(U_+(0))}{\partial t} - \frac{\partial F(U_-(0))}{\partial t}. \quad (4.47)$$

This predicts which direction the shock  $x = x(t)$  moves toward.

## 5 The resolution of the generalized Riemann problem for weakly coupled systems

In this section we extend the methodology in the previous sections in order to investigate the general hyperbolic system with three or more equations ( $m \geq 3$ ). As is well-known, the system (1.1) is in general not endowed with a coordinate system of Riemann invariants and hence it cannot be reduced to a diagonal

characteristic form analogous to (4.3) for the system of two equations. However, for many physical systems that are called *weakly coupled systems* (WCS) in the present paper, we are still able to use the concept of Riemann invariants in order to resolve rarefaction waves in the generalized Riemann problem. Such systems include the compressible fluid flows, the example of electrophoresis, etc. [8, page 130].

Also we can extend the method of Sect. 4.2 in order to resolve jump discontinuities, shocks and contact discontinuities. Note that the concept of Riemann invariants simplifies the resolution of contact discontinuities.

We assume the Jacobian matrix  $DF = \partial F / \partial U$  has a complete set of right eigenvectors  $\Upsilon_i(U)$

$$DF(U)\Upsilon_i(U) = \lambda_i\Upsilon_i(U), \quad (5.1)$$

where  $\lambda_i, i = 1, \dots, m$ , are the eigenvalues of  $DF$  and ordered as

$$\lambda_1 < \lambda_2 < \dots < \lambda_m. \quad (5.2)$$

In this section, we assume that the rarefaction wave associated with  $\lambda_i$  moves to the left and the jump discontinuity associated with  $\lambda_i$  moves to the right. We further suppose that the limiting values  $(\partial U / \partial x)_l$  of spatial derivatives on the left-hand side of the rarefaction wave, and the limiting values  $(\partial U / \partial x)_r$  on the right-hand side of the jump discontinuity, respectively, are known. The modification needed in other cases will be obvious.

### 5.1 The resolution of rarefaction waves

Since the local structure of the solution of (1.1) and (2.1) is determined by the associated Riemann solution of the corresponding homogeneous hyperbolic conservation laws, we first take a look at the homogeneous case (2.3). An  $i$ -Riemann invariant of (2.3) is a smooth scalar function  $E$  such that

$$DE(U)\Upsilon_i(U) = 0, \quad DE(U) = \left( \frac{\partial E}{\partial u_1}, \dots, \frac{\partial E}{\partial u_m} \right). \quad (5.3)$$

The system (2.3) is endowed with a coordinate system of Riemann invariants if there exist functions  $w_1, \dots, w_m$ , such that for any  $i, j = 1, \dots, m$  with  $i \neq j$ ,  $w_j$  is an  $i$ -Riemann invariant of (2.3), and for every  $1 \leq i \leq m$ ,  $Dw_i(U)\Upsilon_i(U) \neq 0$ . With these Riemann invariants, (2.3) is reduced into a diagonal system

$$\frac{\partial w_i}{\partial t} + \lambda_i(W) \frac{\partial w_i}{\partial x} = 0, \quad W = (w_1, \dots, w_m)^\top, \quad i = 1, \dots, m. \quad (5.4)$$

We refer to [8, Sect. 7.3] for details.

Fix the index  $i$  and assume that  $\lambda_i$  is genuinely nonlinear,

$$\nabla \lambda_i \cdot \Upsilon_i = 1, \quad i = 1, \dots, m. \quad (5.5)$$

Consider the corresponding rarefaction wave  $R_i^A$ , which is a part of the solution of the associated Riemann problem (2.3) subject to the initial data (2.4). We represent it by  $U^A(x, t) = V(x/t)$ ,  $i = 1, \dots, m$ , where

$$\lambda_i(V(\xi)) = \xi, \quad \frac{dV}{d\xi} = \Upsilon_i(V(\xi)), \quad \xi = x/t. \quad (5.6)$$

Now we use the vector  $W$  of Riemann invariants as the state vector. In particular, the functions depending on  $U$  can be expressed in terms of  $W$  without changing their notations. The  $i$ -Riemann invariants,  $w_j$ ,  $j \neq i$ , are constant,  $w_j \equiv A_j$ , across the rarefaction wave  $R_i^A$  so that this rarefaction wave is expressed by using

$$\lambda_i(A_1, \dots, A_{i-1}, w_i, A_{i+1}, \dots, A_m) = x/t, \quad w_j = A_j, \quad j \neq i. \quad (5.7)$$

The genuine nonlinearity of  $\lambda_i$  implies that the equations (5.7) can be inverted,

$$w_i(x, t) = w_i(x/t) = \lambda_i^{-1}(x/t; A_1, \dots, A_{i-1}, A_{i+1}, \dots, A_m). \quad (5.8)$$

All other eigenvalues  $\lambda_j$  can be found as explicit functions of  $x/t$ ,

$$\lambda_j = \lambda_j(A_1, \dots, A_{i-1}, w_i(x/t), A_{i+1}, \dots, A_m), \quad j = 1, \dots, m, \quad j \neq i. \quad (5.9)$$

We see that these properties are exactly the same as those for the two-equation systems in Sect. 4. Hence we are able to treat the resolution of centered rarefaction waves in the same way, thus providing a full solution  $R_i^A(x/t; U_L, U_R)$ .

Next we turn to the solution of the rarefaction wave  $R_i$  in the generalized Riemann problem for the nonhomogeneous system (1.1). With the Riemann invariants as the state vector, the system (1.1) can be transformed as

$$\frac{\partial w_i}{\partial t} + \lambda_i(W) \frac{\partial w_i}{\partial x} = H_i(x, W), \quad i = 1, \dots, m, \quad (5.10)$$

where  $H_i(x, W) = Dw_i(U) \cdot S(x, U)$  and  $U$  is expressed in terms of  $W$ . In order to resolve the general rarefaction wave associated with  $\lambda_i$ , we fix the  $w_i$ -equation and combine a  $w_j$ -equation to form a two-equation system,

$$\begin{aligned} \frac{\partial w_i}{\partial t} + \lambda_i \frac{\partial w_i}{\partial x} &= H_i(x, W), \\ \frac{\partial w_j}{\partial t} + \lambda_j \frac{\partial w_j}{\partial x} &= H_j(x, W), \end{aligned} \quad (5.11)$$

for every  $j \neq i$ ,  $\lambda_j \neq \lambda_i$ . This system is exactly the same as (4.3),  $w_i$  (resp.  $w_j$ ) corresponds to  $\phi$  (resp.  $\psi$ ). We can therefore define two families of characteristic

curves  $C^i : \alpha_i = \text{const.}$  and  $C^j : \alpha_j = \text{const.}$ , respectively, by

$$\frac{dx}{dt} = \lambda_i, \quad \frac{dx}{dt} = \lambda_j, \quad (5.12)$$

where  $\alpha_i$  (resp.  $\alpha_j$ ) corresponds to  $\beta$  (resp.  $\alpha$ ) in Sect. 4.1, see Fig. 3. We use the coordinate transforms  $T_{ij} : (\alpha_i, \alpha_j) \rightarrow (x, t)$  to represent the centered rarefaction wave  $R_i$  and  $T_{ij}^{\text{ass}} : (\alpha_i, \alpha_j) \rightarrow (x_{\text{ass}}, t_{\text{ass}})$  to represent the associated rarefaction wave  $R_i^A$ . In terms of these characteristic coordinates, we have characteristic equations for (5.11),

$$\begin{aligned} \frac{\partial x}{\partial \alpha_j} &= \lambda_i \frac{\partial t}{\partial \alpha_j}, & \frac{\partial w_i}{\partial \alpha_j} &= \frac{\partial t}{\partial \alpha_j} H_i(x, W), \\ \frac{\partial x}{\partial \alpha_i} &= \lambda_j \frac{\partial t}{\partial \alpha_i}, & \frac{\partial w_j}{\partial \alpha_i} &= \frac{\partial t}{\partial \alpha_i} H_j(x, W). \end{aligned} \quad (5.13)$$

We can then follow Lemma 6 and Eq. (4.19) in order to calculate  $(\partial w_j / \partial \alpha_j)(\alpha_i, 0)$  and  $(\partial t_{\text{ass}} / \partial \alpha_j)(\alpha_i, 0)$ , as functions of  $\alpha_i$  at the singularity. In fact, the following lemma is the key ingredient in our treatment of the GRP. As in the case of the linear “geometrical optics” (see Sect. 3) it determines the propagation of the transversal derivative of a Riemann invariant along the “degenerate” characteristic  $\alpha_j = 0$  (at the origin).

**Lemma 15** *Throughout the rarefaction wave  $R_i$  associated with  $\lambda_i$  connecting the head and tail values  $V_L$  and  $V_R$ , see Fig. 4, we have*

$$\frac{\partial t_{\text{ass}}}{\partial \alpha_j}(\alpha_i, 0) = \frac{1}{\alpha_i^L} \exp \left( \int_{\alpha_i^L}^{\alpha_i} \frac{1}{\lambda_j(\xi, 0) - \xi} d\xi \right), \quad (5.14)$$

$$\frac{\partial w_j}{\partial \alpha_j}(\alpha_i, 0) = \frac{\partial w_j}{\partial \alpha_j}(\alpha_i^L, 0) + \int_{\alpha_i^L}^{\alpha_i} -\frac{H_j}{\lambda_i - \lambda_j}(\xi, 0) \cdot \frac{\partial t_{\text{ass}}}{\partial \alpha_j}(\xi, 0) d\xi, \quad j \neq i,$$

where  $\alpha_i^L \leq \alpha_i \leq \alpha_i^R$ ,  $\alpha_i^L$  and  $\alpha_i^R$  are the speeds of the head and tail characteristics of  $R_i^A$ . The initial data is

$$\frac{\partial w_j}{\partial \alpha_j}(\alpha_i^L, 0) = w'_j(\alpha_i^L, 0) + \frac{1}{\alpha_i^L} \left( H_j(0, W(\alpha_i^L, 0)) - \lambda_j(\alpha_i^L, 0) w'_j(\alpha_i^L, 0) \right), \quad (5.15)$$

where  $w'_j = \partial w_j / \partial x$ .

**Remark 16** Note that in (5.15) we have already made a choice for the characteristic coordinate  $\alpha_j$ , the value  $\alpha_j$  is the  $x$ -coordinate of the intersection point

of the characteristic curve with the head characteristic of  $R_i$ . Of course, other convenient choices are also possible.

Following Lemma 15, we express

$$\begin{aligned} \frac{\partial w_j}{\partial \alpha_j}(\alpha_i^R, 0) &= \left( \frac{\partial w_j}{\partial t}(\alpha_i^R, 0) + \lambda_i^R \frac{\partial w_j}{\partial x}(\alpha_i^R, 0) \right) \cdot \frac{\partial t_{\text{ass}}}{\partial \alpha_j}(\alpha_i^R, 0) \\ &= \left( \frac{\lambda_j^R - \lambda_i^R}{\lambda_j^R} \cdot \frac{\partial w_j}{\partial t}(\alpha_i^R, 0) + \frac{\lambda_i^R}{\lambda_j^R} \cdot H_j(0, W(\alpha_i^R, 0)) \right) \cdot \frac{\partial t_{\text{ass}}}{\partial \alpha_j}(\alpha_i^R, 0), \end{aligned} \quad (5.16)$$

where we have used (5.11) and the smoothness of  $w_j$ . Translating the result of Lemma 15 to the  $(x, t)$ -coordinate at the tail characteristic  $\alpha_i = \alpha_i^R$ , we obtain the following lemma.

**Lemma 17** *Assume that the rarefaction wave  $R_i$  associated with  $\lambda_i$  connects the states  $V_L$  and  $V_R$ . Let  $\alpha_i^L$  and  $\alpha_i^R$  be the corresponding characteristic speeds at the head and tail of  $R_i^A$ , respectively. Let  $Dw_j$  be as in (5.3) and denote by  $(\partial U / \partial t)_R$  the value evaluated at the tail characteristic  $\alpha_i = \alpha_i^R$  from the smooth region behind  $R_i$ . Then one obtains,*

$$(Dw_j)_R \left( \frac{\partial U}{\partial t} \right)_R = d_{LR}^j, \quad j \neq i, \quad (5.17)$$

where the constant term  $d_{LR}^j$  is expressed as

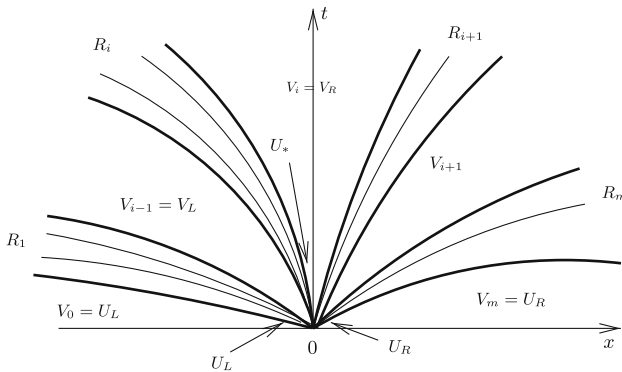
$$d_{LR}^j = \frac{\lambda_j^R}{\lambda_j^R - \lambda_i^R} \left( \frac{\partial w_j}{\partial \alpha_j}(\alpha_i^R, 0) \left( \frac{\partial t_{\text{ass}}}{\partial \alpha_j} \right)^{-1}(\alpha_i^R, 0) - \frac{\lambda_i^R}{\lambda_j^R} H_j(0, W(\alpha_i^R, 0)) \right), \quad (5.18)$$

and  $\lambda_j^R = \lambda_j(\alpha_i^R, 0)$  and  $\lambda_i^R = \alpha_i^R$ .

*Proof* Note that the limiting value of  $\partial w_j / \partial t$  is obtained by Eq. (5.16). Now we use the chain rule for the values in the smooth region behind  $R_i$  to obtain (5.17).

**Remark 18** (Degenerate rarefaction wave or acoustic wave). Note that in the resolution of GRP, all waves must be accounted for. In particular, the  $i$ th wave can just be a characteristic curve, which we regard as a degenerate rarefaction wave or an acoustic wave  $\alpha_i^R = \alpha_i^L$ . All variables  $w_j$ ,  $j = 1, \dots, m$ , are continuous, but in this case  $\partial w_i / \partial t$ ,  $\partial w_i / \partial x$  may experience a jump.

We now proceed to the general derivation of the limiting values (1.6) for the generalized Riemann problem (1.1) and (2.1). We first illustrate this by considering a special case. Assume that the associated Riemann problem (2.3) and (2.4) has a solution of  $m$  rarefaction waves which separate  $m + 1$  constant states, cf. Fig. 4. Let the  $t$ -axis be located inside the intermediate region between the  $i$ -rarefaction wave and the  $(i + 1)$ -rarefaction wave. Then we have the following proposition.



**Fig. 4** Wave configuration for the generalized Riemann problem

**Proposition 19** Assume that the Riemann solution of (1.1) and (2.1) only consists of  $m$  rarefaction waves and that the  $t$ -axis is located inside the intermediate region between the  $i$ th rarefaction wave and the  $(i+1)$ st rarefaction wave. Then  $(\partial U / \partial t)_*$  can be obtained through the following system of linear algebraic equations,

$$\sum_{k=1}^m a_{jk} \left( \frac{\partial u_k}{\partial t} \right)_* = d_j, \quad j = 1, \dots, m, \quad (5.19)$$

where the coefficients  $(a_{j1}, \dots, a_{jm}) = (Dw_j)_*$ , and  $d_j, j = 1, \dots, m$ , depends only on the initial data (2.1) and the Riemann solution  $R^A(\cdot; U_L, U_R)$ .

*Proof* We label by  $I_0, I_1, \dots, I_m$  the regions corresponding to the constant state regions in the associated Riemann problem from the left to the right, as in Fig. 4. We start from the first rarefaction wave associated with  $\lambda_1$ . By Lemma 17, we can obtain the directional derivatives for  $w_j, j = 2, \dots, m$  in the region  $I_1$  across this first rarefaction wave. Successively, we can calculate the derivatives of  $w_j, j = k + 1, \dots, m$  across the  $\lambda_k$ -rarefaction wave,  $k \leq i$ , up to the  $\lambda_i$ -rarefaction wave. Consequently we obtain in the region  $I_i$ ,

$$\sum_{k=1}^m a_{jk} \left( \frac{\partial u_k}{\partial t} \right)_* = d_j, \quad j = i + 1, \dots, m, \quad (5.20)$$

from the left-hand side.

Similarly, we start from the region  $I_m$  for the  $\lambda_m$ th rarefaction wave in the right hand side to get the solution  $w_j, j = 1, \dots, m - 1$ , in the region  $I_{m-1}$ . Successively, we obtain in the region  $I_i$ ,

$$\sum_{k=1}^m a_{jk} \left( \frac{\partial u_k}{\partial t} \right)_* = d_j, \quad j = 1, \dots, i. \quad (5.21)$$



We combine (5.20) and (5.21) to obtain (5.19). Note that  $(a_{j1}, \dots, a_{jm}) = (Dw_j)_*$ . The system (5.19) is uniquely solvable.

*Remark 20* The process of proof actually yields a constructive approach to the calculation of the instantaneous values of time-derivatives along the  $t$ -axis.

As pointed out at the beginning of this section, the system (1.1) is in general not endowed with a coordinate system of Riemann invariants. However, we can still use the concept of the Riemann invariants, as a main ingredient, in the treatment of rarefaction waves for a *weakly coupled system*, which we define next.

We denote by  $L_i(U)$  the left eigenvector associated with  $\lambda_i$  and by  $L(U)$  the left eigenmatrix whose  $i$ th row vector is  $L_i(U)$ . Then we multiply (1.1) from the left by  $L(U)$  to get

$$L(U) \frac{\partial U}{\partial t} + \Lambda(U) L(U) \cdot \frac{\partial U}{\partial x} = L(U) S(x, U), \quad (5.22)$$

where  $\Lambda(U)$  is a diagonal matrix with diagonal entries  $\lambda_i$ . Set

$$W = L(U)U. \quad (5.23)$$

Then (5.22) can be written as

$$\frac{\partial W}{\partial t} + \Lambda(U) \frac{\partial W}{\partial x} = \Pi \left( \frac{\partial U}{\partial t}, \frac{\partial U}{\partial x} \right) + \bar{S}(x, U), \quad (5.24)$$

where

$$\Pi \left( \frac{\partial U}{\partial t}, \frac{\partial U}{\partial x} \right) = \left[ \frac{\partial L(U)}{\partial t} + \Lambda(U) \frac{\partial L(U)}{\partial x} \right] U, \quad \bar{S}(U) = L(U) \cdot S(x, U). \quad (5.25)$$

In general,  $\Pi$  does not vanish. However, suppose that we can split the vector of unknowns  $W$  into two parts,  $W = (W^a, W^b)^\top$ , so that the system (5.24) can be decoupled into two subsystems

$$\begin{aligned} (S_a) : \quad & \frac{\partial W^a}{\partial t} + \Lambda^a(U) \frac{\partial W^a}{\partial x} = \Pi^a \left( \frac{\partial U}{\partial t}, \frac{\partial U}{\partial x} \right) + \bar{S}^a(x, U), \\ (S_b) : \quad & \frac{\partial W^b}{\partial t} + \Lambda^b(U) \frac{\partial W^b}{\partial x} = \Pi^b \left( \frac{\partial U}{\partial t}, \frac{\partial U}{\partial x} \right) + \bar{S}^b(x, U), \end{aligned} \quad (5.26)$$

which satisfy

- (i)  $\Pi^b = 0$ .
- (ii)  $\Pi^a$  does not depend on the derivatives of  $W^a$ .

(iii)  $\Lambda^a(U)$  and  $\Lambda^b(U)$  are diagonal matrices, and

$$\Lambda(U) = \begin{pmatrix} \Lambda^a(U) & 0 \\ 0 & \Lambda^b(U) \end{pmatrix}. \quad (5.27)$$

Thus we can first resolve the rarefaction waves corresponding to the subsystem  $(S_b)$  for  $W^b$  and then resolve the system  $(S_a)$  for  $W^a$ , using the same methodology as in the last subsection. This is the family of *weakly coupled* systems we define below.

**Definition 21** We say that the system (1.1) is *weakly coupled* if there is a coordinate system of *quasi-Riemann invariants*  $W(U) = (W^a(U), W^b(U))^T$  such that (1.1) can be reduced to the *quasi-diagonal* form,

$$\begin{cases} \frac{\partial W^a}{\partial t} + \Lambda^a(W) \frac{\partial W^a}{\partial x} = \Pi^a \left( W, \frac{\partial W^b}{\partial x} \right) + K^a(x, W), \\ \frac{\partial W^b}{\partial t} + \Lambda^b(W) \frac{\partial W^b}{\partial x} = K^b(x, W), \end{cases} \quad (5.28)$$

where  $\Lambda^a$  and  $\Lambda^b$  are diagonal matrices and their entries are the eigenvalues of  $DF$ .

For convenience, we denote

$$\Lambda(W) = \begin{pmatrix} \Lambda^a(W) & 0 \\ 0 & \Lambda^b(W) \end{pmatrix}, \quad \Pi = \begin{pmatrix} \Pi^a \\ 0 \end{pmatrix}, \quad K = \begin{pmatrix} K^a \\ K^b \end{pmatrix}, \quad (5.29)$$

and (5.28) is written as

$$\frac{\partial W}{\partial t} + \Lambda(W) \frac{\partial W}{\partial x} = \Pi \left( W, \frac{\partial W^b}{\partial x} \right) + K(x, W). \quad (5.30)$$

As we shall show later the system of compressible fluid flow is an important example of a weakly coupled system. Also, all systems that can be transformed into a form involving upper triangular coefficient matrix are weakly coupled. Indeed, in this case the above splitting is into  $m$  scalar equations, where the solution procedure resembles the Gaussian elimination. As a result, our problem boils down to solving the diagonal system (5.10).

**Remark 22** (Sonic case) As in Sect. 12, we need to deal with the sonic case that the  $t$ -axis is tangential to the  $i$ -characteristic at the origin  $(x, t) = (0, 0^+)$  for some  $i$ . It is clear that Lemma 17 still holds, where  $\alpha_i^R$  is replaced by  $\alpha_i = 0$ . In addition, we use the  $w_i$ -equation in (5.10), by noting the fact that  $\lambda_i(W^0) = 0$ ,

$W^0 = W(\alpha_i = 0, \alpha_j = 0)$ , to get

$$\left( \frac{\partial w_i}{\partial t} \right) \Big|_{(\alpha_i, \alpha_j) = (0,0)} = H_i(0, W^0). \quad (5.31)$$

It follows that

$$(Dw_i)_0 \left( \frac{\partial U}{\partial t} \right)_* = H_i(0, W^0). \quad (5.32)$$

We summarize these facts in the following theorem (cf. Theorem 13).

**Theorem 23** *Assume that the  $t$ -axis is located in the rarefaction wave associated with the eigenvalue  $\lambda_i$ . Then  $(\partial U / \partial t)_*$  is determined by a system of  $m$  linear equations; the  $m - 1$  equations are given in (5.17) with  $\alpha_i^R = 0$ , and the other one is given by (5.32).*

## 5.2 The resolution of jump discontinuities

We use the same approach as in Sect. 4.2 in order to resolve the jump discontinuity (shock or contact discontinuity) for general systems. Let the jump location be given by  $x = x(t)$  with speed  $\sigma(t) = x'(t)$ . This jump discontinuity is described by the Rankine–Hugoniot jump condition,

$$F(U) - F(\bar{U}) = \sigma(U - \bar{U}), \quad (5.33)$$

where  $U$  and  $\bar{U}$  are the limiting states on two sides, respectively. Let us fix the state  $\bar{U}$ . Then (5.33) is the system of the size  $m$  but with  $m + 1$  unknowns  $U$  and  $\sigma$ . As a standard approach [8], we write (5.33) as

$$\left[ A(U, \bar{U}) - \sigma I \right] (U - \bar{U}) = 0, \quad (5.34)$$

where we are using the Roe matrix

$$A(U, \bar{U}) = \int_0^1 DF(\tau U + (1 - \tau)\bar{U}) d\tau. \quad (5.35)$$

Solving (5.34) yields,

$$\begin{cases} \sigma = \sigma_i(U, \bar{U}), \\ U = \bar{U} + \eta \Gamma_i(U, \bar{U}), \end{cases} \quad (5.36)$$

for a parameter  $\eta \in \mathbb{R}$ , where the  $i$ th jump discontinuity speed  $\sigma_i$  is the eigenvalue of  $A(U, \bar{U})$ , and  $\Gamma_i$  is the associated eigenvector,  $i = 1, \dots, m$ .

For a fixed  $i$ -jump discontinuity, we eliminate  $\eta$  in (5.36) to get  $m - 1$  equations,

$$\Psi_i^j(U, \bar{U}) = 0, \quad j = 1, \dots, m - 1. \quad (5.37)$$

Indeed, this is the system determining the  $i$ th Hugoniot locus in the  $U$  space. We differentiate these equations in the direction of the jump discontinuity  $x = x(t)$ ,  $x'(t) = \sigma_i(U, \bar{U})$ , to get

$$\nabla_U \Psi_i^j(U, \bar{U}) \cdot \left( \frac{\partial U}{\partial t} + \sigma_i \frac{\partial U}{\partial x} \right) = -\nabla_{\bar{U}} \Psi_i^j(U, \bar{U}) \cdot \left( \frac{\partial \bar{U}}{\partial t} + \sigma_i \frac{\partial \bar{U}}{\partial x} \right). \quad (5.38)$$

Denote the limiting values of  $\sigma_i$ ,  $U$ ,  $\bar{U}$ ,  $\partial U / \partial t$  and  $\partial \bar{U} / \partial x$  as  $t$  tends to zero by

$$\begin{aligned} \lim_{t \rightarrow 0^+} \sigma_i &= \sigma_i^0, \quad \lim_{t \rightarrow 0^+} U = U_l, \quad \lim_{t \rightarrow 0^+} \bar{U} = U_r, \\ \lim_{t \rightarrow 0^+} \frac{\partial U}{\partial t} &= \left( \frac{\partial U}{\partial t} \right)_l, \quad \lim_{t \rightarrow 0^+} \frac{\partial \bar{U}}{\partial x} = U'_r. \end{aligned} \quad (5.39)$$

We suppose that the jump discontinuity moves to the right so that  $\sigma_i(U_l, U_r) > 0$ . Our goal is to seek  $(\partial U / \partial t)_l$ . Using (1.1) for smooth solutions, we replace the time derivative  $\partial \bar{U} / \partial t$  by the spatial derivative  $\partial \bar{U} / \partial x$  and replace the spatial derivative  $\partial U / \partial x$  by the time derivative  $\partial U / \partial t$ ,

$$\begin{aligned} \frac{\partial \bar{U}}{\partial t} &= -DF(\bar{U}) \frac{\partial \bar{U}}{\partial x} + S(x, \bar{U}), \\ \frac{\partial U}{\partial x} &= DF(U)^{-1} \left[ -\frac{\partial U}{\partial t} + S(x, U) \right], \end{aligned} \quad (5.40)$$

where we assume that  $DF(U_l)$  is invertible. The case that  $DF(U_l)$  is singular is discussed below in the context of quasi-Riemann invariants. Inserting these relations in (5.38) and taking the time limit we get, for  $j = 1, \dots, m-1$ ,

$$\begin{aligned} &\nabla_U \Psi_i^j(U_l, U_r) [I - \sigma_i^0 DF(U_l)^{-1}] \left( \frac{\partial U}{\partial t} \right)_l \\ &= -\sigma_i^0 \nabla_U \Psi_i^j(U_l, U_r) DF(U_l)^{-1} S(0, U_l) \\ &\quad - \nabla_{\bar{U}} \Psi_i^j(U_l, U_r) [(\sigma_i^0 I - DF(U_r)) U'_r + S(0, U_r)]. \end{aligned} \quad (5.41)$$

Note that this is a system of  $m-1$  linearly independent algebraic equations with  $m$  unknowns  $(\partial U / \partial t)_l$ . This leads to the following lemma for the resolution of the  $i$ -shock.

**Lemma 24** *Let the jump discontinuity  $x = x(t)$  be associated with the eigenvalue  $\lambda_i$ , the related limiting states are denoted in (5.39). Then at the singularity point  $(x, t) = (0, 0)$  we have*

$$\sum_{q=1}^m a_{iq}^j \left( \frac{\partial u_q}{\partial t} \right)_l = d_i^j, \quad j = 1, \dots, m-1, \quad (5.42)$$

where all coefficients  $a_{iq}^j$  and  $d_i^j$  are given explicitly by,

$$\begin{aligned}(a_{i1}^j, \dots, a_{im}^j) &= \nabla_U \Psi_i^j(U_l, U_r) [I - \sigma_i^0 DF(U_l)^{-1}] \\ d_i^j &= -\sigma_i^0 \nabla_U \Psi_i^j(U_l, U_r) DF^{-1}(U_l) S(0, U_l) \\ &\quad - \nabla_{\bar{U}} \Psi_i^j(U_l, U_r) \left[ (\sigma_i^0 I - DF(U_r)) U_r' + S(0, U_r) \right].\end{aligned}\quad (5.43)$$

Now we turn to the case of a weakly coupled system (5.30), as in Definition 21, and work with the quasi-Riemann invariants  $W = (w_1, \dots, w_m)$ . Then (5.37) can be written as

$$\Phi_i^j(W; \bar{W}) = 0, \quad j = 1, \dots, m-1. \quad (5.44)$$

We use the same approach as above to differentiate (5.44) in the direction of the jump discontinuity  $x = x(t)$ , express  $\partial W / \partial x$  by  $\partial W / \partial t$  and  $\partial \bar{W} / \partial t$  by  $\partial \bar{W} / \partial x$  using (5.30),

$$\begin{aligned}\nabla_W \Phi_i^j \cdot \left( \frac{\partial W}{\partial t} + \sigma_i \frac{\partial W}{\partial x} \right) &= -\nabla_{\bar{W}} \Phi_i^j \cdot \left( \frac{\partial \bar{W}}{\partial t} + \sigma_i \frac{\partial \bar{W}}{\partial x} \right), \\ \frac{\partial W}{\partial x} &= \Lambda(W)^{-1} \cdot \left[ -\frac{\partial W}{\partial t} + \bar{\Pi} \left( W, \frac{\partial W^b}{\partial t} \right) + K(x, W) \right], \\ \frac{\partial \bar{W}}{\partial t} &= -\Lambda(\bar{W}) \cdot \frac{\partial \bar{W}}{\partial x} + \Pi \left( \bar{W}, \frac{\partial \bar{W}^b}{\partial x} \right) + K(x, \bar{W}),\end{aligned}\quad (5.45)$$

where  $\bar{\Pi}(W, \partial W^b / \partial t) = \Pi(W, \Lambda^b(W)^{-1} \cdot (-\frac{\partial W^b}{\partial t} + K^b(x, W)))$ , and non-zero eigenvalues are assumed. Indeed, once some eigenvalue  $\lambda_k$  ( $k \neq i$ ) is zero in the limit  $t \rightarrow 0^+$ , we have from (5.30),

$$\frac{\partial w_k}{\partial t} = \Pi_k \left( W, \frac{\partial W^b}{\partial x} \right) + K_k(x, W), \quad k \neq i. \quad (5.46)$$

Then the limiting value of  $\partial w_k / \partial t$  is known, and we just need to consider the reduced (5.45) in terms of the other variables  $w_j, j \neq k$ . For the simplicity in presentation, we therefore assume that all eigenvalues are not zero. Incorporating the last two identities of (5.45) into the first one, we have,

$$\begin{aligned}\nabla_W \Phi_i^j \left[ (I - \sigma_i \Lambda(W)^{-1}) \frac{\partial W}{\partial t} + \sigma_i \Lambda(W)^{-1} \cdot \bar{\Pi} \left( W, \frac{\partial W^b}{\partial t} \right) \right] \\ = -\nabla_W \Phi_i^j \cdot \sigma_i \cdot \Lambda(W)^{-1} \cdot K(x, W) \\ - \nabla_{\bar{W}} \Phi_i^j \left[ (\sigma_i I - \Lambda(\bar{W})) \frac{\partial \bar{W}}{\partial x} + K(x, \bar{W}) + \Pi(W, \partial W^b / \partial x) \right].\end{aligned}\quad (5.47)$$

By taking the limit  $t \rightarrow 0^+$ , we obtain (in analogy to (5.41)),

$$\begin{aligned} \nabla_W \Phi_i^j(W_l, W_r) & \left[ (I - \sigma_i^0 \Lambda(W_l)^{-1}) \left( \frac{\partial W}{\partial t} \right)_l + \sigma_i^0 \Lambda(W_l)^{-1} \cdot \bar{\Pi} \left( W_l, \left( \frac{\partial W^b}{\partial t} \right)_l \right) \right] \\ & = -\nabla_W \Phi_i^j(W_l, W_r) \cdot \sigma_i^0 \cdot \Lambda(W_l)^{-1} \cdot K(0, W_l) \\ & \quad - \nabla_{\bar{W}} \Phi_i^j(W_l, W_r) \left[ (\sigma_i^0 I - \Lambda(W_r)) W_r' + K(0, W_r) + \Pi(W_r, (W_r^b)') \right]. \end{aligned} \quad (5.48)$$

This is a system of  $m - 1$  algebraic equations with  $m$  unknowns  $(\partial w_k / \partial t)_l$ ,  $k = 1, \dots, m$ . Note that the  $i$ th term of the matrix  $I - \sigma_i^0 \Lambda(W_l)^{-1}$  may be zero. Therefore we let  $(\partial w_i / \partial t)_l$  be a free undetermined parameter, and we obtain a system of  $m - 1$  equations for the limiting values  $(\partial w_k / \partial t)_l$ ,  $k \neq i$ , which is given by the following lemma.

**Lemma 25** *Consider the weakly coupled system (5.30). Let the jump discontinuity  $x = x(t)$  be associated with  $\lambda_i$ ,  $\sigma_i^0 = x'(0) > 0$ . Then at the singularity point  $(x, t) = (0, 0)$ , we have the following connections between the vector  $(\partial W / \partial t)_l$  of time derivatives on the left hand side of the jump discontinuity and the spatial derivatives  $W_r' := (\partial W / \partial x)_r$  on the right hand side,*

$$\begin{aligned} \sum_{q=1}^m \frac{\partial \Phi_i^j}{\partial w_q} \cdot \frac{\lambda_q(W_l) - \sigma_i^0}{\lambda_q(W_l)} \cdot \left( \frac{\partial w_q}{\partial t} \right)_l \\ + \sum_{q=1}^m \frac{\partial \Phi_i^j(W_l, W_r)}{\partial w_q} \cdot \frac{1}{\lambda_q(W_l)} \cdot \bar{\Pi}_q \left( W_l, \left( \frac{\partial W^b}{\partial t} \right)_l \right) = d_i^j, \end{aligned} \quad (5.49)$$

where  $j = 1, \dots, m - 1$ , and  $d_i^j$  are given explicitly by,

$$\begin{aligned} d_i^j = & - \sum_{q=1}^m \frac{\partial \Phi_i^j(W_l, W_r)}{\partial w_q} \cdot \frac{\sigma_i^0}{\lambda_q(W_l)} \cdot K_q(0, W_l) \\ & - \sum_{q=1}^m \frac{\partial \Phi_i^j(W_l, W_r)}{\partial \bar{w}_q} \cdot \left[ (\sigma_i^0 - \lambda_q(W_r)) W_r' + K_q(0, W_r) + \Pi_q(W_r, (W_r^b)') \right]. \end{aligned} \quad (5.50)$$

The system (5.49) is an algebraic system for  $(\partial w_k / \partial t)_l$ ,  $k \neq i$ , with the value  $(\partial w_i / \partial t)_l$  being an independent parameter.

**Remark 26** Lemmas 24 and 25 show that we can either use the primitive variables  $U$  or the quasi-Riemann invariants  $W$  for weakly coupled systems in resolving jump discontinuities. The choice of either approach depends on the practical convenience.

**Remark 27** (Weak jump) As in Remark 18, in the limit that the strength of the  $i$ -th shock becomes zero ( $W_l = W_r$ ), the shock trajectory  $x = x(t)$  degenerates to a characteristic curve and  $\lambda_i(W_l) = \sigma_i^0 = \lambda_i(W_r)$ . The term containing  $(\partial w_i / \partial t)_l$  is kicked out in (5.49). Finally we get  $(\partial w_j / \partial t)_l = (\partial w_j / \partial t)_r$  and  $(\partial w_j / \partial x)_l = (\partial w_j / \partial x)_r$ ,  $j \neq i$ . However,  $(\partial w_i / \partial t)_l \neq (\partial w_i / \partial t)_r$ .

### 5.3 Remarks on the resolution of contact discontinuities

In the last subsection we have resolved the jump discontinuities, including contact discontinuities associated with linearly degenerate eigenvalues. However, when the system (1.1) is endowed with a coordinate system of Riemann invariants, as written in (5.10), the situation becomes much simpler for contact discontinuities.

Assume that the eigenvalue  $\lambda_i$  is linearly degenerate and the corresponding contact discontinuity is  $x = x(t)$ . By the definition of Riemann invariants, see (5.3), we see that the Riemann invariant  $w_j$ , associated with  $\lambda_i$ , is continuous across the contact discontinuity  $x = x(t)$ ,  $x'(t) = \sigma_i(U, \bar{U}) = \lambda_i(U) = \lambda_i(\bar{U})$ ,

$$w_j(U) = w_j(\bar{U}), \quad j \neq i. \quad (5.51)$$

Using the same approach as in the last subsection, we differentiate  $w_j$  in the direction of  $x = x(t)$  to yield

$$\frac{\partial w_j(U)}{\partial t} + \lambda_i(U) \frac{\partial w_j(U)}{\partial x} = \frac{\partial w_j(\bar{U})}{\partial t} + \lambda_i(\bar{U}) \frac{\partial w_j(\bar{U})}{\partial x}. \quad (5.52)$$

Using (5.10), we have

$$\begin{aligned} \frac{\partial w_j(U)}{\partial x} &= \frac{1}{\lambda_j(U)} \left[ -\frac{\partial w_j(U)}{\partial t} + H_j(x, W(U)) \right], \\ \frac{\partial w_j(\bar{U})}{\partial t} &= -\lambda_j(\bar{U}) \frac{\partial w_j(\bar{U})}{\partial x} + H_j(x, W(\bar{U})). \end{aligned} \quad (5.53)$$

Note that if  $\lambda_j(U) = 0$ ,  $(\partial w_j / \partial t)_l = H(0, W_l)$ , and we do not need the above manipulation. Thus we assume that  $\lambda_j(U_l) \neq 0$  so that we use (5.53) in (5.52) and take the time limit to obtain (see (5.39) for notations),

$$\left( \frac{\partial w_j}{\partial t} \right)_l := \frac{\lambda_j^l}{\lambda_j^l - \lambda_i^l} \left[ (\lambda_i^r - \lambda_j^r)(w_j)'_r + H_j(0, W_r) - \frac{\lambda_i^l}{\lambda_j^l} H_j(0, W_l) \right], \quad (5.54)$$

where  $\lambda_j^l = \lambda_j(U_l)$ ,  $(w_j)'_r = (\partial w_j / \partial x)_r$ , etc. Thus we obtain the time derivative  $(\partial w_j / \partial t)_l$  provided that  $(w_j)'_r$  and the associated Riemann solution are known. Then the time derivative  $(\partial U / \partial t)_l$  follows. We summarize the above to give the following result.

**Lemma 28** *Let the contact discontinuity  $x = x(t)$  be associated with  $\lambda_i$  and separate two limiting states  $W_l$  and  $W_r$ . Then we have*

$$Dw_j(U_l) \cdot \left( \frac{\partial U}{\partial t} \right)_l = d_j^{rl}, \quad j \neq i, \quad (5.55)$$

where the quantity  $d_j^{rl}$  is expressed explicitly as

$$d_j^{rl} = \frac{\lambda_j^l}{\lambda_j^l - \lambda_i^l} \left[ (\lambda_i^r - \lambda_j^r)(w_j)_r' + H_j(0, W_r) - \frac{\lambda_i^l}{\lambda_j^l} H_j(0, W_l) \right]. \quad (5.56)$$

#### 5.4 The time derivative of solutions at the singularity

In this final subsection we wrap up the calculation of the GRP solution  $(\partial U / \partial t)_*$ , see (2.2). We assume that the rarefaction waves, shocks and contact discontinuities can be resolved with the approach in Sects. 5.1–5.3, and that the local wave pattern at the origin, determined by the associated Riemann solution of (2.3) and (2.4), consists of  $m$  waves. If the  $t$ -axis is located on one side of all waves, the value of  $(\partial U / \partial t)_*$  can be obtained upwind. Therefore, we assume that the  $t$ -axis is located inside the intermediate region between the  $i$ th wave and  $(i + 1)$ st wave. The strategy of the computation of  $(\partial U / \partial t)_*$  is analogous to Proposition 19, but at present, the treatment depends on the type of the  $j$ th wave ( $j = 1, \dots, m$ ); a rarefaction wave, a shock or a contact discontinuity. As has been pointed out, the local wave pattern is determined by the associated Riemann solution  $R^A(x/t; U_L, U_R)$ , see Proposition 1.

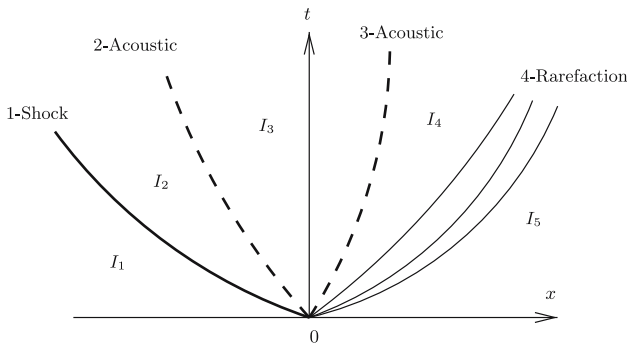
**Theorem 29** *Consider the generalized Riemann problem for the weakly coupled system (5.28). Then the solution  $(\partial U / \partial t)_*$  can be obtained by solving a system of linear algebraic equations*

$$\sum_{k=1}^m a_{jk} \left( \frac{\partial u_k}{\partial t} \right)_* = d_j, \quad j = 1, \dots, m. \quad (5.57)$$

The coefficients  $a_{jk}$  and  $d_j$  are determined constructively from the initial data (2.1) and the associated Riemann solution  $R^A(0; U_L, U_R)$ .

*Proof* The basic idea of the proof, and, indeed, the cornerstone of the GRP methodology, is identical to that of Proposition 19, where all  $m$  waves were assumed to be rarefaction wave. In fact, the initial slopes (2.1) are “rotated” through the various waves emanating from the origin so as to yield the desired  $(\frac{\partial U}{\partial t})_*$ . We first observe that the results of Sect. 5.1 (rarefaction waves) and Sects. 5.2–5.3 (jump discontinuities) can be summarized as follows. Given the limiting values (at  $(x, t) = (0, 0)$ ) of the temporal and spatial derivatives of the unknowns (expressed either by  $U$  or the quasi-Riemann invariants  $W$ ) on one



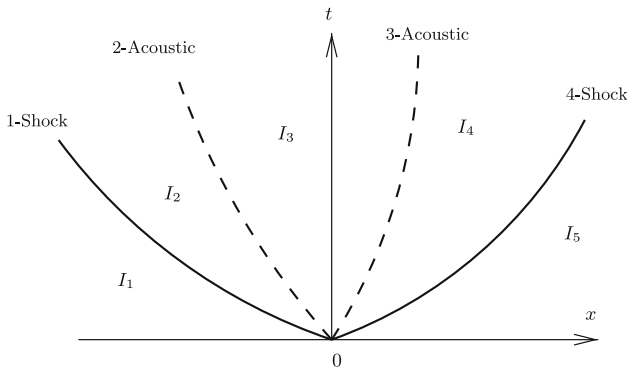


**Fig. 5** An example for a two-wave degenerate pattern for four-equation system: A shock of first family wave moves to the left and a rarefaction wave of fourth family moves to the right

side of the discontinuity, we find  $(m - 1)$  equations for the (limiting values of the) temporal derivatives on the other side (the spatial derivatives are then obtained from the system (1.1)). In other words, “crossing” a single wave we are left with one free parameter in a system of  $m$  equations for the derivatives (on the side labelled as “unknown”). Suppose now that the  $t$ -axis is located between the  $i$ th and  $(i + 1)$ st waves. Counting from the left ( $x < 0$ ) we get for  $(\frac{\partial U}{\partial t})_*$  a system of  $m$  equations, with  $i$  free parameters. Similarly, approaching from the right ( $x > 0$ ) we cross  $(m - i)$  waves, and thus get another system of  $m$  equations, containing  $(m - i)$  free parameters. Eliminating the total of  $m$  free parameters from the two systems of  $m$  equations we obtain precisely the system claimed in the theorem.

Note that in the sonic case, where the  $t$ -axis is “imbedded” in a rarefaction wave, the proof is simpler and the full system is determined by the data on one side.

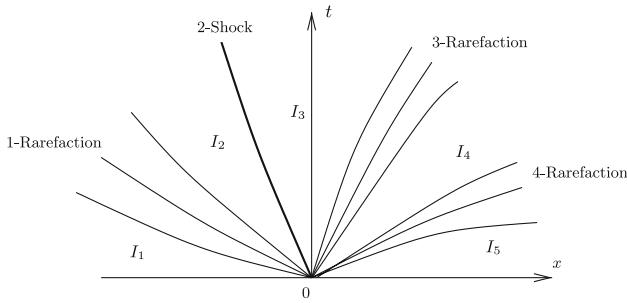
To illustrate our procedure, we examine a few examples in the case of a system of four equations ( $m = 4$ ). The use of quasi-Riemann invariants enables us to simplify the general procedure above (with free parameters) as follows. First we consider a degenerate example of two waves, as in Fig. 5: A shock associated with  $\lambda_1$  moves to the left and a rarefaction wave associated with  $\lambda_4$  moves to the right, the dashed curves represent the acoustic waves associated with  $\lambda_3$  and  $\lambda_4$ , respectively. Applying Lemma 17, we get the limiting values of the derivatives for  $w_1$ ,  $w_2$  and  $w_3$  in the region  $I_4$  by resolving the four-rarefaction wave. Note (Remarks 18 and 27) that out of these derivatives only the derivatives of  $w_1$  and  $w_2$  are continuous across the three-acoustic wave. Hence we get the limiting values  $(\partial w_1 / \partial t)_*$  and  $(\partial w_2 / \partial t)_*$  in the region  $I_3$ . On the other hand, across the one-shock we have three equations for the limiting values of four unknowns  $\partial w_i / \partial t$ ,  $i = 1, 2, 3, 4$ , in the region  $I_2$ , see Lemma 25. Since the derivatives of  $w_1$ ,  $w_3$  and  $w_4$  are continuous across the two-acoustic wave and  $(\partial w_1 / \partial t)_*$  is already known, we can solve the three equations for the limiting values of the unknowns  $\partial w_i / \partial t$ ,  $i = 2, 3, 4$ , in the region  $I_2$ . Then these limiting values for  $i = 3, 4$  are equal to  $(\partial w_3 / \partial t)_*$  and  $(\partial w_4 / \partial t)_*$  in the region  $I_3$ , respectively.



**Fig. 6** An example for a two-wave degenerate pattern for four-equation system: two shocks of first and fourth families move to the left and right, respectively

The second example consists of two shocks, as in Fig. 6. In this case the four-rarefaction wave of the previous example is replaced by a four-shock. We use Lemma 25 (see (5.49)) to obtain three equations for the limiting values of the four unknowns  $\partial w_i / \partial t$  in the region  $I_2$  by resolving the one-shock, and another set of three equations for the limiting values of the four unknowns  $\partial w_i / \partial t$  in the region  $I_4$  by resolving the four-shock,  $i = 1, 2, 3, 4$ . Since  $\partial w_i / \partial t$ ,  $i = 1, 3, 4$ , are continuous across the two-acoustic wave and  $\partial w_i / \partial t$ ,  $i = 1, 2, 4$ , are continuous across the three-acoustic wave, we finally obtain six equations with the four unknowns  $(\partial w_i / \partial t)_*$ ,  $i = 1, 2, 3, 4$ , in the region  $I_3$  and the other two unknown limiting values  $\partial w_2 / \partial t$  in the region  $I_2$  and  $\partial w_3 / \partial t$  in the region  $I_4$ .

We assume for the third example, as in Fig. 7, that the local wave configuration consists of four waves: Two rarefaction waves propagate to the right, a rarefaction wave and a shock move to the left, the  $t$ -axis is located in the intermediate region  $I_3$ . With the results in Sect. 5.1, we can get the limiting values of  $\partial w_1 / \partial t$ ,  $\partial w_2 / \partial t$  and  $\partial w_3 / \partial t$  in the region  $I_4$  by resolving the four-rarefaction wave. Then the limiting values of  $\partial w_1 / \partial x$ ,  $\partial w_2 / \partial x$  and  $\partial w_3 / \partial x$  are obtained by using (5.10). We continue to resolve the three-rarefaction wave to get the limiting value  $(\partial w_1 / \partial t)_*$  and  $(\partial w_2 / \partial t)_*$  in the intermediate region  $I_3$ . Analogously, we can resolve the one-rarefaction wave from the left-hand side to get the limiting values of  $\partial w_2 / \partial t$ ,  $\partial w_3 / \partial t$  and  $\partial w_4 / \partial t$  (resp. the limiting values of  $\partial w_2 / \partial x$ ,  $\partial w_3 / \partial x$  and  $\partial w_4 / \partial x$  again by using (5.10)) in the region  $I_2$ . Then we proceed to resolve the two-shock to obtain  $(\partial w_3 / \partial t)_*$  and  $(\partial w_4 / \partial t)_*$  in the intermediate region  $I_3$ . Recall (Lemma 25) that there are three equations connecting the limiting values of derivatives of  $w_i$ ,  $i = 1, 2, 3, 4$ . Note that the limiting values of the derivatives for  $w_2$ ,  $w_3$  and  $w_4$  in the region  $I_2$  are determined by the treatment of the one-rarefaction wave, leaving there the limiting value of  $\partial w_1 / \partial t$  as a free parameter. Using the (already known) limiting values  $(\partial w_1 / \partial t)_*$  and  $(\partial w_2 / \partial t)_*$  in the region  $I_3$ , we have three equations for three unknowns; the limiting value of  $\partial w_1 / \partial t$  in the region  $I_2$  as well as  $(\partial w_3 / \partial t)_*$  and  $(\partial w_4 / \partial t)_*$  in the region  $I_3$ . Solving these we get  $(\partial w_3 / \partial t)_*$  and  $(\partial w_4 / \partial t)_*$  in  $I_3$ .



**Fig. 7** An example for a full four-wave pattern for four-equation system: two rarefaction waves move to the right, and a rarefaction wave and a shock move to the left

Once we solve the resulting system of linear equations to get  $(\partial w_i / \partial t)_*$ ,  $i = 1, 2, 3, 4$ , we immediately obtain  $(\partial U / \partial t)_*$  in the intermediate region  $I_3$ .

## 6 The acoustic approximation and the $G_1$ -scheme

The acoustic approximation makes sense if the jump at the singularity point  $(x, t) = (0, 0)$  is sufficiently small. Assume that the initial variables  $U(x, 0)$  in (2.1) are continuous at  $x = 0$  while their slopes are not;  $U_L = U_R$  and  $U'_L \neq U'_R$ . Then the Riemann solution to the associated Riemann problem is constant  $R^A(x/t; U_L, U_R) \equiv U_L = U_R$ . Therefore the initial wave pattern does not contain a jump discontinuity (shock) or a centered rarefaction wave. The “waves” emanating from the origin  $(x, t) = (0, 0)$  are acoustic, and therefore their speeds are  $\lambda_i(U_L) = \lambda_i(U_R)$ ,  $i = 1, \dots, m$ .

Denote  $U_* = U_L = U_R$ . Then we can linearize (1.1) around  $U = U_*$  to get

$$\frac{\partial U}{\partial t} + DF(U_*) \frac{\partial U}{\partial x} = S(x, U_*). \quad (6.1)$$

With this linear system of equations, we can use the customary methods, as in Sect. 3, to get the derivative  $(\partial U / \partial t)_*$ : Diagonalize the system (6.1), calculate the derivatives upwind and return to the primitive variables  $(\partial U / \partial t)_*$ .

In our GRP scheme, the initial data (2.1) has a jump discontinuity, and we can solve the generalized Riemann problem (1.1) and (2.1) analytically to calculate the time derivative of solution, as has been summarized in Sect. 5.4. This leads to the scheme which we label as the  $G_\infty$  scheme.

In practice, when  $U_L - U_R$  is sufficiently small, we can simplify this process by resorting to the acoustic case. Setting the Riemann solution  $U_* = R^A(0; U_L, U_R)$  as the background solution, we linearize the system (1.1) to get the linear system (6.1). Diagonalize the system to arrive at

$$\frac{\partial W}{\partial t} + \Lambda(W_*) \frac{\partial W}{\partial x} = L(W_*) S(x, W_*) =: H(x, W_*), \quad (6.2)$$

where  $W = L(U_*)U$ ,  $L = (L_1, \dots, L_m)^\top$ ,  $L_i$  is the left (row) eigenvector associated with  $\lambda_i$ , and  $\Lambda$  is a diagonal matrix with entries  $\lambda_i(U_*)$ . Therefore we can calculate the time derivative of  $W$ , as in the scalar case,

$$\left(\frac{\partial W}{\partial t}\right)_* = \lim_{t \rightarrow 0^+} \frac{\partial W}{\partial t}(0, t) = - \left[ \frac{|\Lambda| + \Lambda}{2} W'_L + \frac{|\Lambda| - \Lambda}{2} W'_R \right] + H(x, W_*), \quad (6.3)$$

where  $|\Lambda| = \text{diag}(|\lambda_1|, \dots, |\lambda_m|)$ . This is an  $O(\Delta t)$  approximation of the time derivatives appearing in (1.5). Returning to the original variables  $U$  we get

$$\left(\frac{\partial U}{\partial t}\right)_* = L^{-1}(U_*) \left(\frac{\partial W}{\partial t}\right)_*. \quad (6.4)$$

The resulting scheme is labelled as the  $G_1$ -scheme. In the original GRP scheme [4], there are the corresponding  $E_1$  (Eulerian) scheme and  $L_1$  (Lagrangian) scheme. Observe that when  $U'_L = U'_R = 0$ , the scheme degenerates to the Godunov scheme. Thus the  $G_1$ -scheme is the simplest possible extension of the Godunov scheme. Once the Godunov scheme is implemented, the implementation of the  $G_1$ -scheme adds a negligible amount of computational effort.

## 7 Several examples in applications

In this section we use the methodology developed above in order to treat several well-known physical examples. Our first two examples, the system of isentropic compressible fluid flow and the system of rotating shallow water equations, are endowed with coordinate systems of Riemann invariants so that they can be treated by the method of Sect. 4. The third example, the system of nonisentropic compressible fluid flow in a duct of variable cross-section, does not possess a full coordinate system of Riemann invariants although there exist Riemann invariants for each characteristic field. However, this system falls into the category of weakly coupled systems, as defined in Definition 21.

### 7.1 Isentropic compressible fluid flow

The system of one-dimensional isentropic flow in gas dynamics is given by

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0, \quad \frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u^2 + p(\rho))}{\partial x} = 0, \quad (7.1)$$

where  $\rho \geq 0$  is the density,  $u$  is the velocity, and  $p(\rho) = a\rho^\gamma$  is the pressure,  $a > 0$  and  $\gamma > 1$  are given constants. The system (7.1) has two eigenvalues

$$\lambda_- = u - c, \quad \lambda_+ = u + c, \quad (7.2)$$

where  $c$  is the speed of sound, given by  $c^2 = a\gamma\rho^{\gamma-1}$ . The two Riemann invariants are taken as

$$\phi = u - \frac{2c}{\gamma - 1}, \quad \psi = u + \frac{2c}{\gamma - 1}, \quad (7.3)$$

where  $\phi$  is associated with  $\lambda_+$ , and  $\psi$  is associated with  $\lambda_-$ . In terms of these Riemann invariants, the system (7.1) is reduced to a diagonal system (see (4.3))

$$\frac{\partial \phi}{\partial t} + \lambda_- \frac{\partial \phi}{\partial x} = 0, \quad \frac{\partial \psi}{\partial t} + \lambda_+ \frac{\partial \psi}{\partial x} = 0. \quad (7.4)$$

We consider a typical local wave pattern consisting of a rarefaction wave moving to the left and a shock moving to the right, and assume that the  $t$ -axis is located inside the intermediate region, as in Fig. 1. However, note that there is no contact discontinuity in the present case. In order to resolve the rarefaction wave, we need to set up the associated characteristic coordinates  $(\alpha, \beta)$ . Taking  $(\alpha, \beta)$  as in Sect. 4, we obtain the following explicit expressions,

$$t_{\text{ass}}(\alpha, \beta) = \frac{\alpha}{(\psi_L - \beta)^{\frac{1}{2\mu^2}}}, \quad x_{\text{ass}}(\alpha, \beta) = \frac{\alpha\beta}{(\psi_L - \beta)^{\frac{1}{2\mu^2}}}, \quad \mu^2 = \frac{\gamma - 1}{\gamma + 1}. \quad (7.5)$$

In [5], we use the same characteristic coordinates. This is because the associated rarefaction wave is isentropic.

The Hugoniot loci for shocks are given by

$$\sigma = \frac{\rho u - \bar{\rho} \bar{u}}{\rho - \bar{\rho}}, \quad u = \bar{u} \pm \left( \frac{1}{\bar{\rho} \bar{p}} \cdot (p(\rho) - p(\bar{\rho}))(\rho - \bar{\rho}) \right)^{\frac{1}{2}} := \bar{u} \pm \Phi(\rho, \bar{\rho}), \quad (7.6)$$

where  $\sigma(t) = x'(t)$  is the shock speed,  $(\bar{\rho}, \bar{u})$  and  $(\rho, u)$  are the preshock and postshock states, respectively.

The following proposition is a straightforward application of Theorems 3 and 13.

**Proposition 30** *Consider the system (7.1) subject to the piecewise initial data (2.1). Assume a typical wave pattern consisting of a rarefaction wave propagating to the left and a shock moving to the right. Then the limiting values  $(\partial \rho / \partial t)_*$  and  $(\partial u / \partial t)_*$  (see (2.2)) are determined by a pair of linear equations,*

$$\begin{aligned} a_L \left( \frac{\partial u}{\partial t} \right)_* + b_L \left( \frac{\partial \rho}{\partial t} \right)_* &= d_L, \\ a_R \left( \frac{\partial u}{\partial t} \right)_* + b_R \left( \frac{\partial \rho}{\partial t} \right)_* &= d_R. \end{aligned} \quad (7.7)$$

The coefficients  $a_L$ ,  $b_L$ ,  $d_L$ ,  $a_R$ ,  $b_R$ ,  $d_R$  are given explicitly in the following two cases.

(i) **Non-sonic case** When the  $t$ -axis is located inside the intermediate region between the rarefaction wave and the shock, we have the non-sonic case,

$$\begin{aligned} a_L &= 1, \quad b_L = \frac{c_*}{\rho_*}, \quad d_L = -(u_* + c_*) \left( \frac{c_*}{c_L} \right)^{\frac{1}{2\mu^2}-1} \left( u'_L + \frac{c_L}{\rho_L} \rho'_L \right), \\ a_R &= 1 - \frac{\sigma_0 u_*}{u_*^2 - c_*^2} - \frac{\partial \Phi}{\partial \rho} \cdot \frac{\sigma_0 \rho_*}{u_*^2 - c_*^2}, \quad b_R = \frac{\sigma_0}{u_*^2 - c_*^2} \cdot \frac{c_*^2}{\rho_*} - \frac{\partial \Phi}{\partial \rho} \cdot \left( 1 - \frac{\sigma_0 u_*}{u_*^2 - c_*^2} \right), \\ d_R &= \frac{3(\sigma_0 - u_R)^2 + c_R^2}{2(\sigma_0 - u_R)} \cdot u'_R - \frac{(\sigma_0 - u_R)^2 + 3c_R^2}{2\rho_R} \rho'_R, \end{aligned} \quad (7.8)$$

and

$$\sigma_0 = \frac{\rho_* u_* - \rho_R u_R}{\rho_* - \rho_R}, \quad \frac{\partial \Phi}{\partial \rho} = \frac{(\sigma_0 - u_*)^2 + c_*^2}{2\rho_*(\sigma_0 - u_*)}. \quad (7.9)$$

(ii) **Sonic case** When the  $t$ -axis (the cell interface) is located inside the rarefaction wave associated with  $\lambda_-$ , we have the sonic case. The coefficients  $a_L$ ,  $b_L$  and  $d_L$  are given in (7.8) in which  $(\rho_*, u_*, c_*)$  is replaced by  $(\rho_0, u_0, c_0)$  there (such that  $c_0 - u_0 = 0$ , cf. Sect. 12), and  $a_R$ ,  $b_R$ ,  $d_R$  are given by

$$a_R = 1.0, \quad b_R = -\frac{c_0}{\rho_0}, \quad d_R = 0.0. \quad (7.10)$$

## 7.2 Rotating shallow water equations with Coriolis force

We consider the shallow water motion on the rotating plane without dependence on one of the coordinates (say,  $y$ ). This system was investigated in [6] and references therein. We use this system to illustrate the performance of our GRP scheme. The governing system can be written in the following form,

$$\begin{aligned} \frac{\partial h}{\partial t} + \frac{\partial(hu)}{\partial x} &= 0, \\ \frac{\partial(hu)}{\partial t} + \frac{\partial(hu^2 + gh^2/2)}{\partial x} &= fhv, \\ \frac{\partial(hv)}{\partial t} + \frac{\partial(huv)}{\partial x} &= -fhu, \end{aligned} \quad (7.11)$$

where  $h$  is the height of water,  $u$ ,  $v$  are two components of the velocity,  $f$  is the (constant) Coriolis force coefficient,  $g$  is the gravitational constant. Note that the first two equations (with  $f = 0$ ) are actually the one-dimensional shallow water model [13] and they are equivalent to the one-dimensional isentropic system (7.1), where  $h$  is regarded as  $\rho$  and  $\gamma = 2$ . A difference from (7.1) is the weak coupling with the other velocity component  $v$  through the source terms, while  $v$  is transported with the velocity  $u$ . Another difference is that there is a

contact discontinuity associated with the eigenvalue  $u$ , across which  $h$  and  $u$  are continuous, and  $v$  has a jump.

The system (7.11) has the Riemann invariants  $v$ , and

$$\phi = u - 2c, \quad \psi = u + 2c, \quad (7.12)$$

where  $c = \sqrt{gh}$ . The pairs  $(v, \psi)$ ,  $(v, \phi)$  and  $(\phi, \psi)$  are, respectively, associated with the eigenvalues  $\lambda_- = u - c$ ,  $\lambda_+ = u + c$  and  $u$ . They comprise a coordinate system of Riemann invariants of the system (7.11). In terms of  $\phi$ ,  $\psi$  and  $v$ , we reduce (7.11) to the characteristic (diagonal) form,

$$\frac{\partial \phi}{\partial t} + \lambda_- \frac{\partial \phi}{\partial x} = fv, \quad \frac{\partial \psi}{\partial t} + \lambda_+ \frac{\partial \psi}{\partial x} = fv, \quad \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} = -fu. \quad (7.13)$$

Since the genuinely nonlinear eigenvalues  $u - c$  and  $u + c$  are the same as those for (7.1), we can use the same characteristic coordinates as in (7.5) when  $\gamma = 2$ . That is, throughout the rarefaction wave associated with  $u - c$ , the characteristic coordinates  $(\alpha, \beta)$  are expressed as

$$t_{\text{ass}}(\alpha, \beta) = \frac{\alpha}{(\psi_L - \beta)^{\frac{3}{2}}}, \quad x_{\text{ass}}(\alpha, \beta) = \frac{\alpha\beta}{(\psi_L - \beta)^{\frac{3}{2}}}. \quad (7.14)$$

In analogy with Proposition 30, we immediately have the limiting values  $(\partial h / \partial t)_*$  and  $(\partial u / \partial t)_*$ . However, there is a small difference due to the presence of source terms in the current case. Also, we have the third wave (contact discontinuity) associated with  $u$ . As we see in the following propositions, this additional wave imposes no difficulty in the resolution of rarefaction waves and shocks.

**Proposition 31** *Assume the configuration as shown in Fig. 1. Then we obtain the time derivatives  $(\partial h / \partial t)_*$  and  $(\partial u / \partial t)_*$  by solving the same system of form (7.7) with  $\rho$  replaced by  $h$  and  $\gamma = 2$ . The coefficients  $a_L$ ,  $b_L$ ,  $a_R$  and  $b_R$  are given in (7.8), while  $d_L$  and  $d_R$  are given as follows.*

(i) *For the non-sonic case, we have*

$$\begin{aligned} d_L &= -(u_* + c_*) \cdot \left( \frac{c_*}{c_L} \right)^{\frac{1}{2}} \left( u'_L + \frac{c_L}{\rho_L} \rho'_L \right) + fv_L, \\ d_R &= \frac{3(\sigma_0 - u_R)^2 + c_R^2}{2(\sigma_0 - u_R)} \cdot u'_R - \frac{(\sigma_0 - u_R)^2 + 3c_R^2}{2\rho_R} \rho'_R \\ &\quad + fv_R \left[ 1 - \frac{\sigma_0}{u_*^2 - c_*^2} \cdot \frac{\sigma_0^2 - u_*^2 + c_*^2}{2(\sigma_0 - u_*)} \right]. \end{aligned} \quad (7.15)$$

(ii) For the sonic case,  $d_L$  is given in (7.15), and  $d_R$  is given as

$$d_R = fv_L. \quad (7.16)$$

Next we treat the variable  $v$ . Note that for the associated Riemann problem,  $v = v_L$  across the rarefaction wave, and  $v = v_R$  across the shock. For the case of the GRP (i.e., the initial data for  $v$  is piecewise linear), we have the following result for  $(\partial v / \partial t)_*$ .

**Proposition 32** Assume the configuration in Fig. 1. Then we have:

- (i) if  $u_* > 0$ , the value  $(\partial v / \partial t)_*$  is obtained from the rarefaction wave (left hand) side,

$$\begin{aligned} \left( \frac{\partial v}{\partial t} \right)_* &= -Fr_* \left( \frac{c_*}{c_L} \right)^3 c_L v'_L \\ &+ fFr_* \left[ -u_L + 3c_* \left( 1 - \left( \frac{c_*}{c_L} \right)^2 \right) \right. \\ &\quad \left. - 2c_L \left( 1 - \left( \frac{c_*}{c_L} \right)^3 \right) + (u_* - c_*) \right], \end{aligned} \quad (7.17)$$

where the Froude number  $Fr_* = u_*/c_*$ ;

- (ii) if  $u_* < 0$ , the value  $(\partial v / \partial t)_*$  is calculated from the shock (right hand) side,

$$\left( \frac{\partial v}{\partial t} \right)_* = \frac{u_*(\sigma_0 - u_R)}{u_* - \sigma_0} [v'_R + f], \quad (7.18)$$

where  $\sigma_0$  is the initial speed of the shock wave.

*Proof* When  $u_* > 0$ , we see that  $v$  is continuous to the left of the contact discontinuity  $\frac{dx}{dt} = u$ . We can use the same method as in Lemmas 6 and 7: Using the characteristic coordinates  $(\alpha, \beta)$  and taking  $v$  as a Riemann invariant, we first calculate  $\partial v / \partial \alpha(0, \beta)$  and then return to express the derivatives of  $v$  with respect to  $x$  and  $t$ , yielding (7.17).

When  $u_* < 0$ , we use the continuity property of  $v$  across the shock and differentiate along the shock trajectory  $x = x(t)$  to get

$$\frac{\partial v(x(t) - 0, t)}{\partial t} + \sigma(t) \frac{\partial v(x(t) - 0, t)}{\partial x} = \frac{\partial v(x(t) + 0, t)}{\partial t} + \sigma(t) \frac{\partial v(x(t) + 0, t)}{\partial x}, \quad (7.19)$$

where  $\sigma(t)$  is the shock speed. Using the equation for  $v$  in (7.13), substituting the spatial derivative of  $v$  in the postshock side by the time derivative and the time derivative in the preshock side by the spatial derivative, we then take the limit to obtain (7.18).



### 7.3 A variable area duct flow

We now consider the variable area duct flow governed by the system [4, Chap. 4]

$$\begin{aligned}\frac{\partial(A(x)\rho)}{\partial t} + \frac{\partial(A(x)\rho u)}{\partial x} &= 0, \\ \frac{\partial(A(x)\rho u)}{\partial t} + \frac{\partial(A(x)\rho u^2)}{\partial x} + A(x)\frac{\partial p}{\partial x} &= 0, \\ \frac{\partial(A(x)\rho E)}{\partial t} + \frac{\partial(A(x)u(\rho E + p))}{\partial x} &= 0,\end{aligned}\tag{7.20}$$

where the variables  $\rho, u, p$  and  $E$  are the density, velocity, pressure and the total specific energy. The total specific energy consists of two parts  $E = \frac{u^2}{2} + e$ ,  $e$  is the internal specific energy. The function  $A(x)$  is the area of the duct. When  $A(x) \equiv 1$ , the system (7.20) represents the planar compressible Euler equations. Let  $T$  be the temperature. Then the entropy  $S$  can be defined, as usual, by the second law of thermodynamics,

$$TdS = de - \frac{p}{\rho^2}d\rho.\tag{7.21}$$

In terms of  $\rho, u$  and  $S$ , the system (7.20) can be written, for smooth flows, as,

$$\begin{aligned}\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + \rho \frac{\partial u}{\partial x} &= -\frac{A'(x)}{A(x)}\rho u, \\ \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \frac{1}{\rho} \frac{\partial p}{\partial x} &= 0, \\ \frac{\partial S}{\partial t} + u \frac{\partial S}{\partial x} &= 0,\end{aligned}\tag{7.22}$$

where  $p$  is regarded as a function of  $\rho$  and  $S$ . We discuss the case of polytropic gases, for which the internal energy  $e = \frac{p}{(\gamma-1)\rho}$ . Then in terms of  $\rho, u$  and  $p$ , the third equation of (7.22) can be replaced by,

$$\frac{\partial p}{\partial t} + u \frac{\partial p}{\partial x} + \rho c^2 \frac{\partial u}{\partial x} = -\frac{A'(x)}{A(x)}\rho c^2 u.\tag{7.23}$$

Here  $c$  is the local speed of sound, given by  $c^2 = \frac{\gamma p}{\rho}$ . Note that (7.22) is just valid for smooth flows. For non-smooth flows, we need to use the conservative form (7.20) with the conserved variables  $(\rho, \rho u, \rho E)$ .

The system (7.20), or equivalently (7.22), possesses three eigenvalues

$$\lambda_- = u - c, \quad \lambda_0 = u, \quad \lambda_+ = u + c.\tag{7.24}$$

We introduce two variables  $\phi, \psi$  [5],

$$\phi = u - \int \frac{c(\omega, S)}{\omega} d\omega, \quad \psi = u + \int \frac{c(\omega, S)}{\omega} d\omega. \quad (7.25)$$

The functions  $\phi, \psi$  can be expressed in terms of total differentials, see [5, Eqs. (2.6), (2.10) and (2.15)]

$$d\phi = du - \frac{1}{\rho c} dp - \frac{T}{c} dS, \quad d\psi = du + \frac{1}{\rho c} dp + \frac{T}{c} dS. \quad (7.26)$$

For the entropy  $S$ , we have

$$TdS = \frac{dp}{(\gamma - 1)\rho} - \frac{c^2}{(\gamma - 1)\rho} d\rho. \quad (7.27)$$

The three pairs  $(\psi, S)$ ,  $(u, p)$  and  $(\phi, S)$  are the Riemann invariants associated with  $\lambda_-$ ,  $\lambda_0$  and  $\lambda_+$ , respectively. However, there is no full coordinate system of Riemann invariants so that (7.20) cannot be reduced to a diagonal form. At this point, the system (7.20) is substantially different from the system of isentropic flow (7.1) and the system of shallow water equations (7.11). However, it falls into the category of weakly coupled systems, as defined in Definition 21. Indeed, we take  $\phi, \psi$  and  $S$  as the (quasi)-Riemann invariants to write (7.22) as

$$\begin{cases} \frac{\partial \phi}{\partial t} + (u - c) \frac{\partial \phi}{\partial x} = B_1, \\ \frac{\partial \psi}{\partial t} + (u + c) \frac{\partial \psi}{\partial x} = B_2, \\ \frac{\partial S}{\partial t} + u \frac{\partial S}{\partial x} = 0. \end{cases} \quad (7.28)$$

where  $B_1 = T \frac{\partial S}{\partial x} + \frac{A'(x)}{A(x)} cu$ ,  $B_2 = T \frac{\partial S}{\partial x} - \frac{A'(x)}{A(x)} cu$ . For the present system,  $W^a = (\phi, \psi)^\top$  and  $W^b = S$ , corresponding to Definition 21.

We use this weakly coupled form to resolve the generalized Riemann problem for (7.20) subject to piecewise linear initial data of the form (2.1). Assume that the configuration is as shown in Fig. 1; a rarefaction wave associated with  $u - c$  moves to the left, a shock associated with  $u + c$  moves to the right, and the  $t$ -axis is located inside the intermediate region. Denote by  $p_*$ ,  $u_*$  the limiting values of  $p$ ,  $u$  at the contact discontinuity as  $t \rightarrow 0_+$ . Similarly, denote by  $\rho_{*1}$ ,  $c_{*1}$  and  $\rho_{*2}$ ,  $c_{*2}$  the limiting values of  $\rho$ ,  $c$  on the left-hand and right-hand sides of the contact discontinuity, respectively. Then we resolve the rarefaction wave, the shock and the contact discontinuity, separately.

First we resolve the rarefaction wave associated with  $u - c$  from the left. According to the general treatment of weakly coupled system in Sect. 5, this

is done by first treating  $W^b$  and solving for  $W^a$ . In our case, it means that we are using the Riemann invariants  $\phi, \psi$  with appropriate dependence on  $S$ . Due to the special form of the system, the dependence of  $S$  is very simple. For this purpose, we need to establish the system of characteristic coordinates  $(x, t) \rightarrow (\alpha, \beta)$ , where  $\alpha$  and  $\beta$  are defined in terms of the eigenvalues  $u + c$ ,  $u - c$ , respectively. See Fig. 1 and the section of Fig. 3. The associated characteristic coordinates  $t_{\text{ass}}(\alpha, \beta)$ ,  $x_{\text{ass}}(\alpha, \beta)$  are given in (7.5). In the limit  $\alpha \rightarrow 0$ ,  $u(0, \beta) - c(0, \beta) = \beta$  so that  $c = \mu^2(\psi_L - \beta)$  and  $u = (\mu^2 - 1)(\psi_L - \beta) + \psi_L$ , where  $\mu^2 = \frac{\gamma-1}{\gamma+1}$ ,  $\psi_L = \psi(\rho_L, u_L, p_L)$ . Equations (7.4) are replaced by the first two equations of (7.28). According to Lemma 17, we obtain  $\partial\psi/\partial t$  and  $\partial S/\partial t$ , as stated in the following proposition.

**Proposition 33** *Assume that the rarefaction wave associated with  $u - c$  moves to the left, as in Fig. 1. Consider the Riemann invariants  $S, \psi$  and their time derivatives  $\partial S/\partial t$ ,  $\partial\psi/\partial t$  as continuous functions of  $\alpha, \beta$ , in the rectangle  $-\alpha_0 \leq \alpha \leq 0$ ,  $\beta_L \leq \beta \leq \beta_*$  for some  $\alpha_0 > 0$ . Then we have,*

$$\begin{aligned} T \frac{\partial S}{\partial t}(0, \beta) &= -(\beta + c_L \theta) \theta^{\frac{2\gamma}{\gamma-1}} T_L S'_L, \quad \theta = c(0, \beta)/c_L, \\ \frac{\partial \psi}{\partial t}(0, \beta) &= H_1 + \frac{A'(0)}{2A(0)} H_2, \end{aligned} \quad (7.29)$$

where  $T_L S'_L$  is defined by (7.27), and  $H_1, H_2$  are given by,

$$\begin{aligned} H_1 &= -\frac{\beta + c_L \theta}{c_L} \theta^{\frac{\gamma+1}{\gamma-1}} T_L S'_L + \frac{\beta + 2c_L \theta}{c_L} \theta^{\frac{3-\gamma}{2(\gamma-1)}} \left[ \frac{2\gamma}{3\gamma-1} T_L S'_L - c_L \psi'_L \right], \\ H_2 &= \beta(\beta + c_L \theta) - (\beta + 2c_L \theta) \left[ u_L \theta^{\frac{3-\gamma}{2(\gamma-1)}} + \overline{H}_2 \right], \\ \overline{H}_2 &= \begin{cases} \frac{-2(\gamma+1)c_L \theta}{(\gamma-1)(3\gamma-5)} \left( 1 - \theta^{\frac{5-3\gamma}{2(\gamma-1)}} \right) - \frac{(\gamma+1)\psi_L}{\gamma-3} \left[ 1 - \theta^{\frac{3-\gamma}{2(\gamma-1)}} \right], & \text{if } \gamma \neq 3, 5/3, \\ 2c_L(\theta - 1) - \psi_L \ln \theta, & \text{if } \gamma = 3, \\ 2[c_L \theta \ln \theta + \psi_L(1 - \theta)], & \text{if } \gamma = 5/3. \end{cases} \end{aligned} \quad (7.30)$$

*Proof* According to the general treatment of Sect. 5, we need to consider the evolution of the time derivatives of two pairs of Riemann invariants  $(\phi, S)$  and  $(\phi, \psi)$ .

(i) **The computation of  $T\partial S/\partial t$**  we use the first and third equations of (7.28) to form a system of two equations,

$$\begin{cases} \frac{\partial \phi}{\partial t} + (u - c) \frac{\partial \phi}{\partial x} = B_1, \\ \frac{\partial S}{\partial t} + (u + c) \frac{\partial S}{\partial x} = c \frac{\partial S}{\partial x}. \end{cases} \quad (7.31)$$

Then, in terms of  $\alpha$  and  $\beta$ , we have (since  $\partial x/\partial \alpha = (u - c)\partial t/\partial \alpha$  and  $\partial x/\partial \beta = (u + c)\partial t/\partial \beta$ ),

$$\begin{aligned}\frac{\partial S}{\partial \beta} &= \frac{\partial t}{\partial \beta} \cdot \left[ \frac{\partial S}{\partial t} + (u + c) \frac{\partial S}{\partial x} \right] = \frac{\partial t}{\partial \beta} \cdot c \frac{\partial S}{\partial x}, \\ \frac{\partial S}{\partial \alpha} &= \frac{\partial t}{\partial \alpha} \left[ \frac{\partial S}{\partial t} + (u - c) \frac{\partial S}{\partial x} \right] = -\frac{\partial t}{\partial \alpha} \cdot c \frac{\partial S}{\partial x}.\end{aligned}\quad (7.32)$$

We note, as in (4.16), that

$$\frac{\partial^2 t}{\partial \alpha \partial \beta}(0, \beta) = \frac{1}{2c(0, \beta)} \frac{\partial t}{\partial \alpha}(0, \beta), \quad (7.33)$$

where we have used the fact that  $\lambda_-(0, \beta) = \beta$ ,  $\lambda_-(0, \beta) - \lambda_+(0, \beta) = -2c(0, \beta)$  and  $(\partial t/\partial \beta)(0, \beta) = 0$ . Thus, differentiating the first equation of (7.32) with respect to  $\alpha$  and noting  $\frac{\partial t}{\partial \beta}(0, \beta) \equiv 0$ , we get

$$\frac{\partial}{\partial \beta} \left( \frac{\partial S}{\partial \alpha}(0, \beta) \right) = \frac{1}{2} \frac{\partial t}{\partial \alpha}(0, \beta) \cdot \frac{\partial S}{\partial x}(0, \beta) = -\frac{1}{2c(0, \beta)} \frac{\partial S}{\partial \alpha}(0, \beta). \quad (7.34)$$

Integrating from  $\beta_L$  to  $\beta$  yields,

$$\frac{\partial S}{\partial \alpha}(0, \beta) = \frac{\partial S}{\partial \alpha}(0, \beta_L) \exp \left( - \int_{\beta_L}^{\beta} \frac{1}{2c(0, \eta)} d\eta \right) = \frac{\partial S}{\partial \alpha}(0, \beta_L) \cdot \theta^{\frac{1}{2\mu^2}}. \quad (7.35)$$

Similarly, we get from (7.33)

$$\frac{\partial t}{\partial \alpha}(0, \beta) = \frac{\partial t}{\partial \alpha}(0, \beta_L) \theta^{-\frac{1}{2\mu^2}}. \quad (7.36)$$

In particular, from the second equation of (7.32) and (7.36), we have

$$c(0, \beta) \frac{\partial S}{\partial x}(0, \beta) = -\frac{\partial S}{\partial \alpha}(0, \beta) \cdot \left( \frac{\partial t}{\partial \alpha} \right)^{-1}(0, \beta) = c_L S'_L \theta^{\frac{1}{\mu^2}}. \quad (7.37)$$

Hence using the entropy equation in (7.28), we return to the  $(x, t)$ -coordinate system to get  $T \frac{\partial S}{\partial t}$ ,

$$T(0, \beta) \frac{\partial S}{\partial t}(0, \beta) = -u(0, \beta) T(0, \beta) \frac{\partial S}{\partial x}(0, \beta), \quad (7.38)$$

which gives  $T \frac{\partial S}{\partial t}$  in (7.29) by using (7.37) and noting  $T/T_L = c^2/c_L^2$ .

(ii) **The computation of  $\partial\psi/\partial t$**  We now consider the first two equations in (7.28), i.e., the system of two equations,

$$\begin{cases} \frac{\partial\phi}{\partial t} + (u - c)\frac{\partial\phi}{\partial x} = B_1, \\ \frac{\partial\psi}{\partial t} + (u + c)\frac{\partial\psi}{\partial x} = B_2. \end{cases} \quad (7.39)$$

As in (7.32), we note

$$\frac{\partial\psi}{\partial t} + (u - c)\frac{\partial\psi}{\partial x} = \left(\frac{\partial t}{\partial\alpha}\right)^{-1} \frac{\partial\psi}{\partial\alpha}. \quad (7.40)$$

Regard the source terms as functions of  $(\alpha, \beta)$ . In the limit  $(\alpha \rightarrow 0)$ , they are known from the first part of the proof, see Eq. (7.37). In terms of the general treatment of weakly coupled systems in Sect. 5, this is at the stage where  $W^b (= \{S\})$  is fully resolved, and we can turn to the diagonal system for  $W^a (= \{\phi, \psi\})$ . Following the same reasoning as the one leading up to Eq. (7.34), we get

$$\frac{\partial}{\partial\beta} \left( \frac{\partial\psi}{\partial\alpha}(0, \beta) \right) = \frac{1}{2c(0, \beta)} \cdot \frac{\partial t}{\partial\alpha}(0, \beta) \cdot B_2(0, \beta). \quad (7.41)$$

The integration from  $\beta_L$  to  $\beta$  yields,

$$\frac{\partial\psi}{\partial\alpha}(0, \beta) = \frac{\partial\psi}{\partial\alpha}(0, \beta_L) + \int_{\beta_L}^{\beta} \frac{1}{2c(0, \eta)} \cdot \frac{\partial t}{\partial\alpha}(0, \eta) \cdot B_2(0, \eta) d\eta. \quad (7.42)$$

The initial data for  $\partial\psi/\partial\alpha$  is given by

$$\frac{\partial\psi}{\partial\alpha}(0, \beta_L) = \frac{\partial t}{\partial\alpha}(0, \beta_L) \left[ T_L S'_L - \frac{A'(0)}{A(0)} c_L u_L - 2c_L \psi'_L \right], \quad (7.43)$$

where we note the following relation by using (7.39) and (7.40),

$$\frac{\partial\psi}{\partial\alpha} = \frac{\partial t}{\partial\alpha} \cdot \left[ \frac{\partial\psi}{\partial t} + (u - c)\frac{\partial\psi}{\partial x} \right] = \frac{\partial t}{\partial\alpha} \cdot \left[ B_2 - 2c\frac{\partial\psi}{\partial x} \right]. \quad (7.44)$$

Once we obtain  $(\partial\psi/\partial\alpha)(0, \beta)$  from (7.42), we get

$$2c(0, \beta) \frac{\partial\psi}{\partial x}(0, \beta) = B_2(0, \beta) - \left(\frac{\partial t}{\partial\alpha}\right)^{-1}(0, \beta) \frac{\partial\psi}{\partial\alpha}(0, \beta). \quad (7.45)$$

we insert this into (7.40) to get

$$\frac{\partial \psi}{\partial t}(0, \beta) = -\frac{u-c}{2c} B_2(0, \beta) + \frac{u+c}{2c} \left( \frac{\partial t}{\partial \alpha} \right)^{-1} \frac{\partial \psi}{\partial \alpha}(0, \beta). \quad (7.46)$$

Then using  $B_2(0, \beta) = T(0, \beta) \frac{\partial S}{\partial x}(0, \beta) - \frac{A'(0)}{A(0)} c(0, \beta) u(0, \beta)$  and the value  $\frac{\partial \psi}{\partial \alpha}(0, \beta)$  in (7.42), we obtain the second equation in (7.29).

**Proposition 34** (Resolution of rarefaction waves) *Assume that the rarefaction wave associated with  $u - c$  moves to the left. Use the characteristic coordinates  $(\alpha, \beta)$  as above and consider the limiting values  $\frac{\partial u}{\partial t}(0, \beta)$  and  $\frac{\partial p}{\partial t}(0, \beta)$ ,  $\beta_L \leq \beta \leq \beta_*$ . Then we have*

$$\tilde{a}_L(0, \beta) \frac{\partial u}{\partial t}(0, \beta) + \tilde{b}_L(0, \beta) \frac{\partial p}{\partial t}(0, \beta) = \tilde{d}_L(\beta), \quad (7.47)$$

where the coefficients  $\tilde{a}_L$ ,  $\tilde{b}_L$  and  $\tilde{d}_L$  can be expressed explicitly as follows. With  $\theta = c(0, \beta)/c_L$ ,

$$\tilde{a}_L(0, \beta) = 1, \quad \tilde{b}_L(0, \beta) = \frac{1}{\rho(0, \beta)c(0, \beta)}, \quad (7.48)$$

and

$$\tilde{d}_L(\beta) = \frac{\beta + 2\theta c_L}{c_L} \cdot \theta^{\frac{3-\gamma}{2(\gamma-1)}} \left( \frac{2\gamma}{3\gamma-1} T_L S'_L - c_L \psi'_L \right) + \frac{A'(0)}{2A(0)} H_2, \quad (7.49)$$

where  $H_2$  is given in (7.30).

*Proof* We use (7.26) to get

$$\frac{\partial u}{\partial t} + \frac{1}{\rho c} \frac{\partial p}{\partial t} = \frac{\partial \psi}{\partial t} - \frac{T}{c} \frac{\partial S}{\partial t}. \quad (7.50)$$

The right-hand side can be evaluated at  $(0, \beta)$  using the two equations in (7.29) to yield (7.47) as well.

As in Sect. 5.2, we can use the Riemann invariants  $W$  for the resolution of jump discontinuities. However, as in the first part of Sect. 5.2, it is more convenient to use the basic primitive variables  $U = (\rho, u, p)$ . See Remark 26.

The Rankine–Hugoniot conditions for shocks are

$$\sigma = \frac{\rho u - \bar{\rho} \bar{u}}{\rho - \bar{\rho}}, \quad u = \bar{u} \pm \Phi(p; \bar{p}, \bar{\rho}), \quad \rho = h(p; \bar{p}, \bar{\rho}), \quad (7.51)$$

where  $(\rho, u, p)$  and  $(\bar{\rho}, \bar{u}, \bar{p})$  are the states ahead and behind the shock, respectively, and

$$\Phi(p; \bar{p}, \bar{\rho}) = (p - \bar{p}) \sqrt{\frac{1 - \mu^2}{\bar{\rho}(p + \mu^2 \bar{p})}}, \quad h(p; \bar{p}, \bar{\rho}) = \bar{\rho} \frac{p + \mu^2 \bar{p}}{\bar{p} + \mu^2 \bar{p}}, \quad \mu^2 = \frac{\gamma - 1}{\gamma + 1}. \quad (7.52)$$

Assume that this shock is associated with  $u + c$  and moves to the right, as shown in Fig. 1. Then it can be resolved with a standard method, see [5].

**Proposition 35** (Resolution of shocks) *Assume that a shock associated with  $u + c$  moves to the right. Then the limiting values  $(\partial p / \partial t)_*$  and  $(\partial u / \partial t)_*$  satisfy the linear relations*

$$\tilde{a}_R \left( \frac{\partial u}{\partial t} \right)_* + \tilde{b}_R \left( \frac{\partial p}{\partial t} \right)_* = \tilde{d}_R, \quad (7.53)$$

where the coefficients are given explicitly in the following,

$$\begin{aligned} \tilde{a}_R &= 1 - \frac{\sigma_0 u_*}{u_*^2 - c_{*2}^2} - \frac{\sigma_0 \rho_{*2} c_{*2}^2}{u_*^2 - c_{*2}^2} \cdot \Phi_1, \\ \tilde{b}_R &= \frac{1}{\rho_{*2}} \frac{\sigma_0}{u_*^2 - c_{*2}^2} - \left( 1 - \frac{\sigma_0 u_*}{u_*^2 - c_{*2}^2} \right) \Phi_1, \\ \tilde{d}_R &= L_p^R \cdot p'_R + L_u^R \cdot u'_R + L_\rho^R \cdot \rho'_R + \frac{A'(0)}{A(0)} j_R, \end{aligned} \quad (7.54)$$

and

$$\begin{aligned} L_p^R &= -\frac{1}{\rho_R} + (\sigma_0 - u_R) \cdot \Phi_2, \\ L_u^R &= \sigma_0 - u_R - \rho_R \cdot c_R^2 \cdot \Phi_2 - \rho_R \cdot \Phi_3, \\ L_\rho^R &= (\sigma_0 - u_R) \cdot \Phi_3, \\ j_R &= -(\Phi_2 c_{*2}^2 + \Phi_3) \rho_R u_R + (1 + \Phi_1 \rho_{*2} u_*) \frac{\sigma_0 c_{*2}^2 u_*}{u_*^2 - c_{*2}^2}; \\ \sigma_0 &= \frac{\rho_{*2} u_* - \rho_R u_R}{\rho_{*2} - \rho_R}, \\ \Phi_1 &= \frac{1}{2} \sqrt{\frac{1 - \mu^2}{\rho_R(p_* + \mu^2 p_R)}} \cdot \frac{p_* + (1 + 2\mu^2)p_R}{p_* + \mu^2 p_R}, \\ \Phi_2 &= -\frac{1}{2} \sqrt{\frac{1 - \mu^2}{\rho_R(p_* + \mu^2 p_R)}} \cdot \frac{(2 + \mu^2)p_* + \mu^2 p_R}{p_* + \mu^2 p_R}, \\ \Phi_3 &= -\frac{p_* - p_R}{2\rho_R} \sqrt{\frac{1 - \mu^2}{\rho_R(p_* + \mu^2 p_R)}}. \end{aligned} \quad (7.55)$$

Next we want to resolve the contact discontinuities. Let  $x = x(t)$  be the jump discontinuity. The Rankine–Hugoniot (jump) conditions are

$$u(x(t) - 0, t) = u(x(t) + 0, t), \quad p(x(t) - 0, t) = p(x(t) + 0, t). \quad (7.56)$$

Indeed,  $u$  and  $p$  are the Riemann invariants associated with  $\lambda_0 = u$ . Denote  $D/Dt = \partial/\partial t + u\partial/\partial x$ ,  $u^\pm(t) := u(x(t) \pm 0, t)$ ,  $p^\pm(t) := p(x(t) \pm 0, t)$ . Then along  $x = x(t)$  we have

$$\frac{Du^+(t)}{Dt} = \frac{Du^-(t)}{Dt}, \quad \frac{Dp^+(t)}{Dt} = \frac{Dp^-(t)}{Dt}. \quad (7.57)$$

Note that

$$\begin{aligned} \frac{\partial u}{\partial t} &= \frac{Du}{Dt} + \frac{u}{\rho c^2} \frac{Dp}{Dt} + \frac{A'(x)}{A(x)} u^2, \\ \frac{\partial p}{\partial t} &= \frac{Dp}{Dt} + \rho u \frac{Du}{Dt}. \end{aligned} \quad (7.58)$$

or

$$\begin{aligned} \frac{Du}{Dt} &= \frac{1}{c^2 - u^2} \left[ c^2 \frac{\partial u}{\partial t} - \frac{u}{\rho} \frac{\partial p}{\partial t} - \frac{A'(x)}{A(x)} c^2 u^2 \right], \\ \frac{Dp}{Dt} &= \frac{c^2}{u^2 - c^2} \left[ \rho u \frac{\partial u}{\partial t} - \frac{\partial p}{\partial t} - \frac{A'(x)}{A(x)} \rho u^3 \right]. \end{aligned} \quad (7.59)$$

Then, once the limiting values  $(\partial u/\partial t)_*$  and  $(\partial p/\partial t)_*$  on one side of the contact discontinuity are known, we can obtain them on the other side. We remind that they are different on the two sides since the density  $\rho$  experiences a jump there.

Combining all above discussion, we can solve the generalized Riemann problem (7.20) and (2.1). We summarize our results in the following propositions.

**Proposition 36** (Non-sonic case) *Assume a typical wave configuration for the generalized Riemann problem for (7.20) as shown in Fig. 1. Then we can obtain  $(\partial u/\partial t)_*$  and  $(\partial p/\partial t)_*$  by solving the following pair of linear equations,*

$$\begin{aligned} a_L \left( \frac{\partial u}{\partial t} \right)_* + b_L \left( \frac{\partial p}{\partial t} \right)_* &= d_L, \\ a_R \left( \frac{\partial u}{\partial t} \right)_* + b_R \left( \frac{\partial p}{\partial t} \right)_* &= d_R, \end{aligned} \quad (7.60)$$

where  $a_L$ ,  $b_L$ ,  $d_L$  and  $a_R$ ,  $b_R$ ,  $d_R$  are specified below. Also the computation of  $(\partial \rho/\partial t)_*$  are computed by the following two cases.

(i) If  $u_* > 0$ , the contact discontinuity moves to the right. The coefficients  $a_L$ ,  $b_L$  and  $d_L$  are given in (7.47),

$$(a_L, b_L, d_L) = (\tilde{a}_L, \tilde{b}_L, \tilde{d}_L). \quad (7.61)$$



The coefficients  $a_R$ ,  $b_R$  and  $d_R$  are given by

$$\begin{aligned} a_R &= \frac{c_{*1}^2}{c_{*1}^2 - u_*^2} \left[ \tilde{a}_R \left( 1 - \frac{\rho_{*1} u_*^2}{\rho_{*2} c_{*2}^2} \right) + \tilde{b}_R (\rho_{*2} - \rho_{*1}) u_* \right], \\ b_R &= \frac{1}{c_{*1}^2 - u_*^2} \left[ \tilde{a}_R \left( -\frac{1}{\rho_{*1}} + \frac{c_{*1}^2}{\rho_{*2} c_{*2}^2} \right) u_* - \tilde{b}_R \left( -\frac{\rho_{*2}}{\rho_{*1}} u_*^2 + c_{*1}^2 \right) \right], \\ d_R &= \tilde{d}_R + \frac{A'(0)}{A(0)} \frac{u_*^3}{c_{*1}^2 - u_*^2} \left[ \tilde{a}_R \left( 1 - \frac{\rho_{*1} c_{*1}^2}{\rho_{*2} c_{*2}^2} \right) + \tilde{b}_R (\rho_{*2} - \rho_{*1}) c_{*1}^2 \right]. \end{aligned} \quad (7.62)$$

The value  $(\partial\rho/\partial t)_*$  is computed from the rarefaction side,

$$\left( \frac{\partial\rho}{\partial t} \right)_* = \frac{1}{c_*^2} \left[ \left( \frac{\partial p}{\partial t} \right)_* + (\gamma - 1) \rho_* u_* \left( \frac{c_*}{c_L} \right)^{\frac{1+\mu^2}{\mu^2}} T_L S'_L \right], \quad (7.63)$$

by using the state equation  $p = p(\rho, S)$ .

(ii) If  $u_* < 0$ , the contact discontinuity moves to the left. The coefficients  $a_R$ ,  $b_R$  and  $d_R$  are given in Proposition 35,

$$(a_R, b_R, d_R) = (\tilde{a}_R, \tilde{b}_R, \tilde{d}_R). \quad (7.64)$$

While the coefficients  $a_L$ ,  $b_L$  and  $d_L$  are computed by

$$\begin{aligned} a_L &= \frac{c_{*2}^2}{c_{*2}^2 - u_*^2} \left[ \tilde{a}_L \left( 1 - \frac{\rho_{*2} u_*^2}{\rho_{*1} c_{*1}^2} \right) + \tilde{b}_L (\rho_{*1} - \rho_{*2}) u_* \right], \\ b_L &= \frac{1}{c_{*2}^2 - u_*^2} \left[ \tilde{a}_L \left( -\frac{1}{\rho_{*2}} + \frac{c_{*2}^2}{\rho_{*1} c_{*1}^2} \right) u_* - \tilde{b}_L \left( -\frac{\rho_{*1}}{\rho_{*2}} u_*^2 + c_{*2}^2 \right) \right], \\ d_L &= \tilde{d}_L + \frac{A'(0)}{A(0)} \frac{u_*^3}{c_{*2}^2 - u_*^2} \left[ \tilde{a}_L \left( 1 - \frac{\rho_{*2} c_{*2}^2}{\rho_{*1} c_{*1}^2} \right) + \tilde{b}_L (\rho_{*1} - \rho_{*2}) c_{*2}^2 \right]. \end{aligned} \quad (7.65)$$

The value  $(\partial\rho/\partial t)_*$  is computed from the shock side,

$$g_\rho^R \left( \frac{\partial\rho}{\partial t} \right)_* + g_p^R \left( \frac{Dp}{Dt} \right)_* + g_u^R \left( \frac{Du}{Dt} \right)_* = u_* \cdot f_R, \quad (7.66)$$

where  $g_\rho^R$ ,  $g_p^R$ ,  $g_u^R$  and  $f_R$  are constant, explicitly given in the following,

$$g_\rho^R = u_* - \sigma_0, \quad g_p^R = \frac{\sigma_0}{c_{*2}^2} - u_* H_1, \quad g_u^R = \rho_{2*}(\sigma_0 - u_*) \cdot u_* \cdot H_1,$$

$$f_R = (\sigma_0 - u_R) \cdot H_2 \cdot p'_R + (\sigma_0 - u_R) \cdot H_3 \cdot \rho'_R - \rho_R \cdot (H_2 c_R^2 + H_3) \cdot u'_R \quad (7.67)$$

$$- \frac{A'(0)}{A(0)} \cdot (H_2 c_R^2 + H_3) \rho_R u_R,$$

and  $H_1$ ,  $H_2$  and  $H_3$  are expressed by

$$H_1 = \frac{\rho_R(1 - \mu^4)p_R}{(p_R + \mu^2 p_*)^2}, \quad H_2 = \frac{\rho_R(\mu^4 - 1)p_*}{(p_R + \mu^2 p_*)^2}, \quad H_3 = \frac{p_* + \mu^2 p_R}{p_R + \mu^2 p_*}. \quad (7.68)$$

**Proposition 37** (Sonic case) *Assume that the  $t$ -axis is located inside the rarefaction wave associated with  $u - c$ . Then we have*

$$\left(\frac{\partial u}{\partial t}\right)_0 = \frac{1}{2} \left[ \tilde{d}_L + \theta^{\frac{2\gamma}{\gamma-1}} T_L S'_L + \frac{A'(0)}{A(0)} u_0^2 \right],$$

$$\left(\frac{\partial p}{\partial t}\right)_0 = \frac{\rho_0 c_0}{2} \left[ \tilde{d}_L - \theta^{\frac{2\gamma}{\gamma-1}} T_L S'_L - \frac{A'(0)}{A(0)} u_0^2 \right], \quad (7.69)$$

where  $\tilde{d}_L$  is given in (7.49), with  $\theta = c_0/c_L$ , and  $(u_0, \rho_0, c_0)$  is the limiting value of  $(u, \rho, c)$  along the  $t$ -axis so that  $u_0 - c_0 = 0$ , cf. the sonic case in Proposition 30.

*Proof* Note that at the origin, we have

$$\left(\frac{\partial \phi}{\partial t}\right)_0 = \left(\frac{\partial \phi}{\partial t}\right)_0 + (u_0 - c_0) \left(\frac{\partial \phi}{\partial x}\right)_0 = \left(T \frac{\partial S}{\partial x}\right)_0 + \frac{A'(0)}{A(0)} c_0 u_0. \quad (7.70)$$

That is,

$$\left(\frac{\partial u}{\partial t}\right)_0 - \frac{1}{\rho_0 u_0} \left(\frac{\partial p}{\partial t}\right)_0 = \left(T \frac{\partial S}{\partial x}\right)_0 + \frac{A'(0)}{A(0)} c_0 u_0. \quad (7.71)$$

Since  $(T \partial S / \partial x)_0 = \theta^{\frac{2\gamma}{\gamma-1}} T_L S'_L$ , we use Proposition 34 to complete the proof.

Finally we present the acoustic case that  $U_L = U_R$  but  $U'_L \neq U'_R$ , which leads to the  $G_1$  scheme.

**Proposition 38** (Acoustic case) *Assume that  $U_L = U_R$  and  $U'_L \neq U'_R$ . Then we have the acoustic case, and  $(\partial u/\partial t)_*$  and  $(\partial p/\partial t)_*$  are solved as*

$$\begin{aligned} \left(\frac{\partial u}{\partial t}\right)_* &= -\frac{1}{2} \left[ (u_* + c_*) \left( u'_L + \frac{p'_L}{\rho_* c_*} \right) + (u_* - c_*) \left( u'_R - \frac{p'_R}{\rho_* c_*} \right) \right], \\ \left(\frac{\partial p}{\partial t}\right)_* &= -\frac{\rho_* c_*}{2} \left[ (u_* + c_*) \left( u'_L + \frac{p'_L}{\rho_* c_*} \right) - (u_* - c_*) \left( u'_R - \frac{p'_R}{\rho_* c_*} \right) \right] \\ &\quad - \frac{A'(0)}{A(0)} \rho_* c_*^2 u_*. \end{aligned} \quad (7.72)$$

The quantity  $(\partial \rho/\partial t)_*$  is solved according to the direction of the contact discontinuity,

$$\left(\frac{\partial \rho}{\partial t}\right)_* = \frac{1}{c_*^2} \left[ \left(\frac{\partial p}{\partial t}\right)_* + u_* (p'_L - c_*^2 \rho'_L) \right] \quad (7.73)$$

if  $u_* = u_L = u_R > 0$ ; and

$$\left(\frac{\partial \rho}{\partial t}\right)_* = \frac{1}{c_*^2} \left[ \left(\frac{\partial p}{\partial t}\right)_* + u_* (p'_R - c_*^2 \rho'_R) \right] \quad (7.74)$$

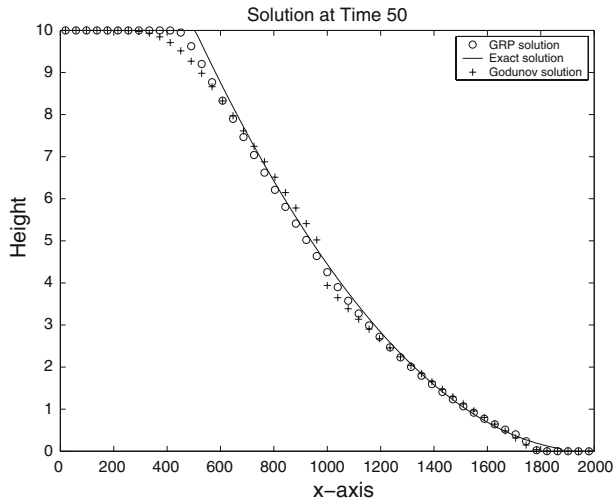
if  $u_* = u_L = u_R < 0$ .

## 8 Numerical examples

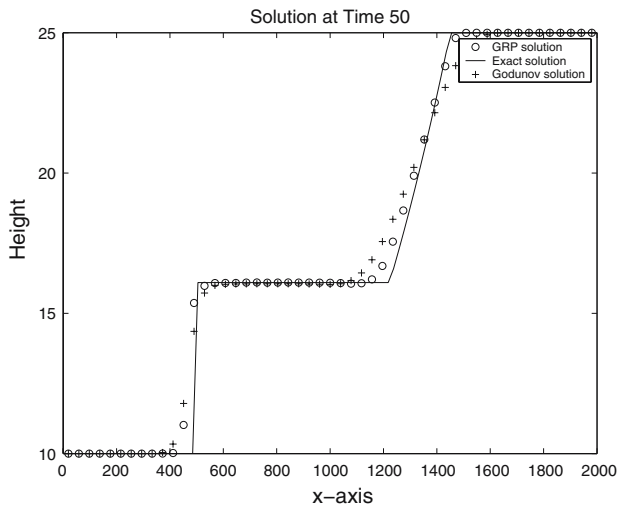
In accord with Sect. 7, we present several numerical examples to show the performance of our GRP scheme.

### 8.1 The Riemann problem for isentropic flows

Two examples are given for isentropic flows (7.1), see Fig. 8, in which fifty grid points are used both for the Godunov scheme and the GRP scheme. Note that (7.1) can be used to model a shallow water motion,  $\rho$  being explained as the height of water with  $\gamma = 2$ . Therefore the first simulates the dam collapse problem with an almost dry bed on one side. We clearly see that the sonic point glitch in the first-order Godunov solution is eliminated by the GRP scheme. Also this example shows that our GRP can preserve the positivity of the height of water. The second is the standard Riemann problem. The solution contains a shock propagating to the left and a rarefaction wave moving to the right. We see the high accuracy of the GRP scheme, particularly for the rarefaction wave, which may be due to its analytic resolution in our GRP scheme. Recall that in [12] the rarefaction wave is replaced by a rarefaction shock.



(a) Dam collapse problem with low height of water:  $a = 4.9$ ,  $\gamma = 2$

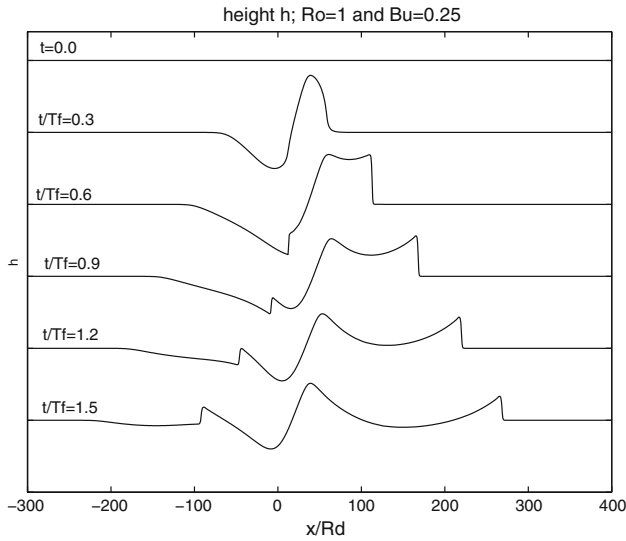


(b) Riemann problem for isentropic flow:  $a = 1$ ,  $\gamma = 1.4$

**Fig. 8** Numerical solutions for isentropic flows. **a** The Riemann initial data are:  $\rho_L = 10.0$ ,  $u_L = 0.0$ ,  $\rho_R = 10^{-5}$ ,  $u_R = 0.0$ . **b** The Riemann initial data are:  $\rho_L = 10.0$ ,  $u_L = 0.0$ ,  $\rho_R = 25$ ,  $u_R = 0.0$

## 8.2 Rotating shallow water equations with Coriolis force

We use our scheme to simulate the classical Rossby problem, which illustrates the evolution of a simple jet-shaped initial momentum imbalance, see [6]. The



**Fig. 9** Shock formation from jets

initial distribution  $h(x, 0) \equiv 10$ ,  $u(x, 0) \equiv 0.0$  and  $v(x, 0) = VN_L(x)$ , where

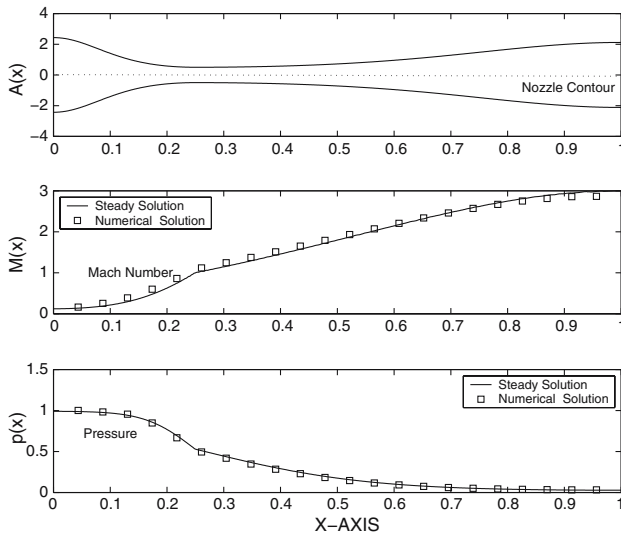
$$N_L(x) = \frac{(1 + \tanh(4x/L + 2)) \cdot (1 - \tanh(4x/L - 2))}{(1 + \tanh(2))^2}, \quad (8.1)$$

and the parameters  $V$  and  $L$  are given by the Rossby number  $Ro = \frac{V}{fL}$  and the Burger number  $Bu = \frac{gh}{f^2 L^2}$ . In Fig. 9, we use  $f = 0.5$ ,  $g = 9.81$ ,  $Ro = 1.0$  and  $Bu = 0.25$ . We observe that two shocks are formed at  $t/T_f = 0.6$ ,  $T_f = 2\pi/f$ , and propagate to the left and to the right from the jet, respectively. One of the shocks is formed within the jet core. The result is totally consistent with that in [6].

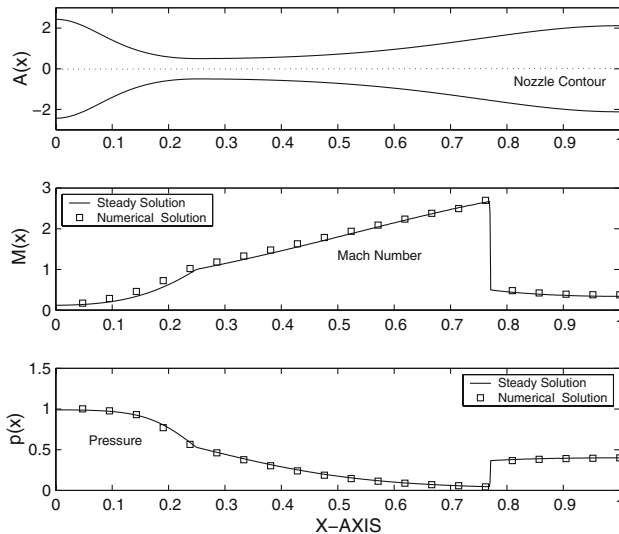
### 8.3 A steady flow in a converging-diverging nozzle

We use the examples in [4, Sect. 6.5] to test the ability of the present scheme to attain the steady state very quickly. Consider a flow in a converging-diverging nozzle, which occupies the interval  $0 \leq x \leq 1$ , and whose cross-sectional area function is given by the following expression,

$$A(x) = \begin{cases} A_{\text{in}} \exp(-\log(A_{\text{in}}) \sin^2(2\pi x)), & 0 \leq x < 0.25, \\ A_{\text{ex}} \exp\left(-\log(A_{\text{ex}}) \sin^2\left(\frac{2\pi(1-x)}{3}\right)\right), & \end{cases} \quad (8.2)$$



**Fig. 10** Large time in the Laval Nozzle. The *solid line* is the steady solution, and the points are the GRP solution with 22 grid points at time  $t = 15.5$

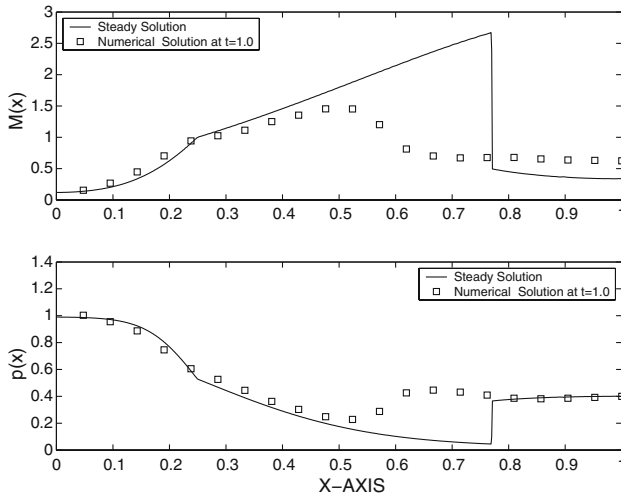


**Fig. 11** Large time in the Laval Nozzle. The *solid line* is the steady solution, and the points are the GRP solution with 22 grid points at time  $t = 15.5$

where  $A_{in} = 4.8643$  and  $A_{ex} = 4.2346$ . The initial data we use are

$$U(x, 0) = \begin{cases} U_L = (\rho_0, 0, p_0), & 0 < r < 0.25, \\ U_R = (\rho_0, 0, \rho_0(p_b/p_0)^\gamma), & 0.25 < r < 1, \end{cases} \quad (8.3)$$

where  $p_b$  is a constant value determined by the steady state solution at  $x = 1$ .



**Fig. 12** Large time in the Laval Nozzle. The solid line is the steady solution, and the points are the GRP solution with 22 grid points at time  $t = 1.0$

For a perfect gas with a polytropic index  $\gamma = 1.4$ , the Mach number  $M(x) = u(x)/c(x)$  is determined by  $A(x)$  through the algebraic relation

$$[A(x)]^2 = \frac{1}{[M(x)]^2} \left[ \frac{2}{\gamma + 2} \left( 1 + \frac{\gamma - 1}{2} [M(x)]^2 \right) \right]^{\frac{\gamma + 1}{\gamma - 1}}. \quad (8.4)$$

Then the steady flow is given by

$$\begin{aligned} p(x) &= p_0 \left[ 1 + \frac{\gamma - 1}{2} [M(x)]^2 \right]^{-\frac{\gamma}{\gamma - 1}}, \\ \rho(x) &= \rho_0 \left[ 1 + \frac{\gamma - 1}{2} [M(x)]^2 \right]^{-\frac{1}{\gamma - 1}}, \\ u(x) &= M(x) \sqrt{\gamma p(x) / \rho(x)}, \end{aligned} \quad (8.5)$$

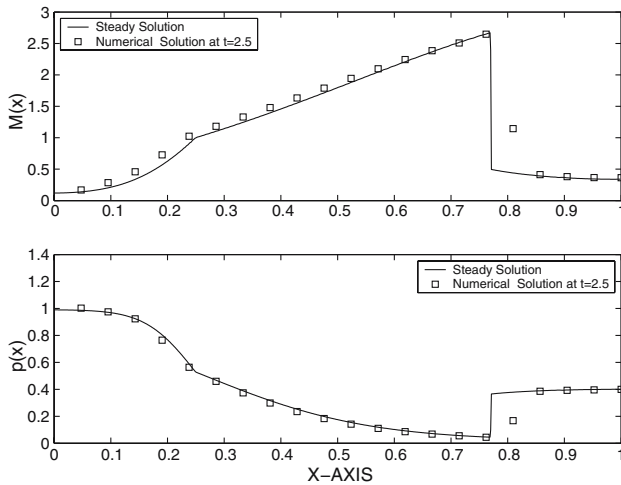
where  $\rho_0$  and  $p_0$  need to be specified.

We consider two cases:

(A) A smooth flow where  $p(1) = 0.0272237$  is obtained from (8.5) by taking  $x = 1$  in (8.4) leading to  $M(1) = 3$ .

(B) Setting  $p(1) = 0.4$  leads to a discontinuous steady state solution, as shown by the solid lines in Fig. 11.

We use the same strategy in [4, Sect. 6.5] to deal with the boundary conditions at  $x = 0$  and 1. In both cases, we use 22 coarse points to display the performance



**Fig. 13** Large time in the Laval Nozzle. The *solid line* is the steady solution, and the points are the GRP solution with 22 grid points at time  $t = 2.5$

of our scheme in Figs. 10 and 11, and see that our GRP solution is in very good agreement with the exact solution.

In order to see how fast our GRP solution converges to the steady state, we display two different time intervals:  $t = 1.0$  and  $2.5$ , see Figs. 12 and 13. It is seen that at time  $t = 2.5$ , our GRP solution almost attains the steady state. These show that our GRP solution can converge to the steady state very quickly.

**Acknowledgements** We would like to thank Professors J. Falcovitz, M. Lukacova, G. Warnecke, P. Zhang and T. Zhang for their interest and many useful discussions. Matania Ben-Artzi is grateful to the School of Mathematics, Capital Normal University for the hospitality during his visit in 2005. Jiequan Li is grateful to the Institute of Mathematics, the Hebrew University of Jerusalem for the hospitality during his visit in 2006 as well as IAN, Magdeburg University the support of Alexander von Humboldt Foundation during his stay from June 2004 to May 2005. This research is also supported by the grant NSFC with no. 10301022, 973 project with no. 2006CB805902, Fok Ying Tong Education Foundation, the Key Program from Beijing Educational Commission with no. KZ200510028018, and Program for New Century Excellent Talents in University (NCET) as well as PHR (IHLB).

## References

1. Ben-Artzi, M., Falcovitz, J.: A second-order Godunov-type scheme for compressible fluid dynamics. *J. Comput. Phys.* **55**(1), 1–32 (1984)
2. Ben-Artzi, M., Falcovitz, J.: An upwind second-order scheme for compressible duct flows. *SIAM J. Sci. Statist. Comput.* **7**(3), 744–768 (1986)
3. Ben-Artzi, M.: The generalized Riemann problem for reactive flows. *J. Comput. Phys.* **81**(1), 70–101 (1989)
4. Ben-Artzi, M., Falcovitz, J.: *Generalized Riemann Problems in Computational Gas Dynamics*. Cambridge University Press, Cambridge (2003)
5. Ben-Artzi, M., Li, J., Warnecke, G.: A direct Eulerian GRP scheme for compressible fluid flows. *J. Comp. Phys.* **218**, 19–43 (2006)



6. Bouchut, F., Le Sommer, J., Zeitlin, V.: Frontal geostrophic adjustment and nonlinear wave phenomena in one dimensional rotating shallow water. Part 2: High resolution numerical simulations. *J. Fluid Mech.* **514**, 35–63 (2004)
7. Bourgeade, A., LeFloch, Ph., Raviart, P.-A.: An asymptotic expansion for the solution of the generalized Riemann problem. II. Application to the equations of gas dynamics. *Ann. Inst. H. Poincaré Anal. Non Linéaire* **6**(6), 437–480 (1989)
8. Dafermos, C.M.: *Hyperbolic Conservation Laws in Continuum Physics*. Springer, Heidelberg (2000)
9. Godunov, S.K.: A finite difference method for the numerical computation and discontinuous solutions of the equations of fluid dynamics. *Mat. Sb.* **47**, 271–295 (1959)
10. Godlewski, E., Raviart, P.-A.: *Numerical approximation of hyperbolic systems of conservation laws*. Appl. Math. Sci. 118, Springer, Heidelberg (1996)
11. Jin, S.: A steady-state capturing method for hyperbolic systems with geometrical source terms. *M2 AN Math. Model. Numer. Anal.* **35**(4), 631–645 (2001)
12. Leer, B. van : Towards the ultimate conservative difference scheme, V. A second-order sequel to Godunov's method. *J. Comput. Phys.* **32**(1), 101–136 (1979)
13. Li, J., Chen, G.: The generalized Riemann problem method for the shallow water equations with bottom topography. *Int. J. Numer. Methods Eng.* **65**(6), 834–862 (2006)
14. Li, T.T.: *Global Classical Solutions for Quasilinear Hyperbolic Systems*. Research in Applied Mathematics. Wiley, Chichester/Masson, Paris (1994)
15. LeFloch, Ph., Raviart, P.-A.: An asymptotic expansion for the solution of the generalized Riemann problem. I. General theory. *Ann. Inst. H. Poincaré Anal. Non Linéaire* **5**(2), 179–207 (1988)
16. Smoller, J.: *Shock Waves and Reaction-Diffusion Equations*, 2nd edn, vol. 258. Springer, New York (1994)
17. Sweby, P.K.: High resolution schemes using flux limiters for hyperbolic conservation laws. *SIAM J. Numer. Anal.* **21**(5), 995–1011 (1984)
18. Toro, E.: *Riemann solvers and numerical methods for fluid dynamics. A practical introduction*. Springer, Berlin (1997)
19. Toro, E.: Derivative Riemann solvers for systems of conservation laws and ADER methods. *J. Comp. Phys.* **212**, 150–165 (2006)